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RESEARCH

GENERAL DYNAMICS CORPORATION ELECTRIC BOAT DIVISION

GENERAL DYNAMICS CORPORATION Electric Boot Division Groton, Connecticut

EXPERIMENTAL EVALUATION
OF THE
EFFECT OF OCEANOGRAPHIC PARAMETERS
ON
SUBMARINE SONAR PERFORMANCE(U)

USS PERMIT (SSN594) AND USS BLUEGILL (SS242)
PACIFIC OCEAN - JANUARY 1966

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ABSTRACT

The results of measuring the effects of environmental variables on acoustic transmission in the ocean are summarized in this report. The environmental variables were measured both before and during a controlled-geometry submarine exercise, using sensors on a research vessel and an aircraft. The acoustic signals were obtained from the submarines. During the submarine exercises, the SUBIC DDP-24 computer was used to predict the best listening depths for each run, using the most recent sound velocity profile data measured from the submarine as the input to a ray-trace program. The interpretation of the acoustic signals in the context of the measured environmental variables is the major result of this report.

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FOREWORD

The work described in this report was performed by the Information Processing Section of the Applied Sciences Department, Electric Boat division of General Dynamics Corporation, as part of the Submarine Integrated Control Program (SUBIC). Electric Boat division is prime contractor and coordinator of this program under contract NOnr 2512(00). Lcdr. W. Billing, USN, is Project Officer for ONR. Dr. R. D. Collier, Senior Staff Scientist, is Project Coordinator for Electric Boat division under the direction of Dr. A. J. van Woerkom, Chief Scientist of the Applied Sciences Department.

The cooperation of Commander, Submarine Squadron Three, his staff and the ship's company of USS PERMIT (SSN594) is gratefully acknowledged.

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INTRODUCTION AND SUMMARY

One of the primary objectives of the SUBIC Research Program is to develop techniques of applying knowledge of the physical ocean environment to the tactical deployment of attack submarines.

An initial approach is to develop display techniques which can be utilized by the submarine commanding officer in decision making. An important development of the recent past is an acoustic ray pattern display of the sound energy generated by a sound source (own ship or target), and the adaption of a high speed, real-time, compact digital computer with cathode ray tube display for implementation of shipboard ray pattern display.

The first use of this computer-display system at sea took place in February 1965 aboard the USS DACE (SSN607) and demonstrated the applicability of ray trace techniques for tactical decisions.

The second use of this system took place in July 1965 aboard the USS TINOSA (SSN606) and further extended ranging techniques.

The need for improved environmental models to provide more realistic inputs to the ray trace program and computations of transmission loss is recognized. For example, the space-time variations in the sound velocity vs. depth profile can introduce significant changes in the ray paths and sound intensities for given depth/range combinations.

The third at-sea test, in January 1966, was designed to measure the environmental variables and their direct effect upon sound propagation. These propagation studies were conducted by the USS PERMIT in conjunction with the USS BLUEGILL (SS242) off the United States West Coast, at which time R/V SEA SERPENT obtained time series measurements of oceanographic parameters. This report describes the results of that experiment.

As planned, the exercise resulted in two sets of data: the signal data from the submarines and the environmental data from the research vessel. The interpretation of the former in the context of the latter was the principal objective of the exercise. How this was done by utilizing the simulation capability of the SUBIC Ray Trace Program constitutes the major result to be reported.

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Briefly, an order of magnitude difference in the variance of the received acoustic signal was recorded at ranges of 5,000 and 10,000 yards (Section III). Furthermore, the variance was smaller at the longer range, discounting volume and surface reverberation as possible explanations. A difference in variance of comparable magnitude was apparent in both passive and active runs, eliminating phase effects of multiple transmission, or other frequency effects, as possible explanations. An explanation was found, however, in the environmental data.

The measurement of the thermal structure of the upper 500 feet of the ocean, taken from the surface ship in the general locale of the submarine exercise, revealed a large scale fluctuation in the depth of the surface sound channel with range (Section Π). The cause of this fluctuation is explained by the overall view of the surface temperature distribution obtained by aircraft infrared thermometer runs.

The ray trace program was recently expanded to include a model of internal waves (Section III). With the proper interpretation, this model was used to simulate the measured variations in the surface channel depth. This simulation resulted in a confirmation of the signal data: that the 5,000-yard data was taken in a region where, because of the particular conditions observed, the variable surface channel would cause considerable fluctuation in the signal with time, while the 10,000-yard data was in a region where, fortuitously for the comparison, the signal strength was practically undisturbed by the varying depth of the channel.

The result is not entirely conclusive. No quantitative comparison is possible from the existing data and a good description of the channel depth was not obtained. Nonetheless, an otherwise unexplainable observation of signal variability, and an observation of such contrast as to be undeniable, is qualitatively explained by the observation of large scale fluctuations in the medium.

Also included (Section IV) are the autocorrelation functions of the signal about its mean. A time scale of the magnitude of a few minutes is indicated for signal coherency and this too can be explained on the basis of the submarines cutting through spatially periodic variations in channel depth of a magnitude commensurate with what was observed.

In summary, although a detailed survey of the area was made at the time of the test, it was far from sufficient to provide all of the data necessary for an absolute calibration of the propagation model. It did, however, show that inhomogenieties did exist in the sound velocity structure and that these were of sufficient magnitude to cause variances in the sonar signal received. In addition, it was determined that the SUBIC at-sea ray trace was applicable to active as well as passive signals in predicting average transmission loss, and that an internal

wave ray trace model programmed on a laboratory computer was able to roughly predict the variance in both the active and passive signals.

The D/E angle was monitored for the first time during a SUBIC at-sea test. The results indicated that the vertical beamwidth is too wide to accurately track a target in the surface channel, thus severely handicapping passive ranging based upon the D/E angle. However, there are indications that a new method of passive ranging based upon the variance in S/N may be developed.

(Page)

OPERATION AREA ENVIRONMENTAL DATA

The main purpose of the presence of the R/V SEA SERPENT and the aircraft during the PERMIT - BLUEGILL tests was to sample the environment in such a way that the variability in S/N and transmission loss as measured by the submarines could be correlated with fluctuations in the oceanographic parameters. In this way, data would be provided for improvement in environmental models used as input to the ray trace program. Although the environmental data collection results were limited, the path for future investigation was indicated.

The surface ship and aircraft sampling programs were designed to provide maximum possible background data on the local oceanographic conditions and to provide detailed data on the variability in the acoustic field during the submarine tests. The surface ship program consisted of tests to determine spalial, temporal and directional characteristics of temperature and sound velocity changes in the test area. In general terms, the surface ship program during the tests was to sample continually on a square track, the dimensions of which corresponded to typical transmission ranges. Each leg of the box was made up of thermistor chain tows, whereas the vertices of the box were stationary thermistor chain recordings and sound velocity profiles. The instrument suite consisted of a thermistor chain, velocimeter and bathythermograph. The aircraft program consisted of gathering data on the gross water mass distribution by using a Barnes IT-2S infrared thermometer to record the distribution and fluctuations in sea surface isotherms. These flights were to take place over the three-day period of the submarine tests and were to cover a 30- by 60-mile area.

The general oceanography of the region has been well established. Water of subarctic origin moves south down the coast of California, becoming modified by atmospheric conditions and entrainment of nearshore coastal water. This south-bound current, the California Current, is an extension of the Aleutian Current and extends from about 48° N to 23° N where it converges with equatorial water. During the winter, from November through January, a countercurrent or eddy is well developed inshore of the California Current. This circulation tends to carry relatively warm saline water northward and has been named the Davidson Current. Beneath the southbound, meandering California Current is a northbound current of equatorial origin.

It was expected that January tracklines running west from the coast at 34 N would pass from the region dominated by northbound water into the southbound water where acoustic conditions were good. Additionally, the track would pass through a frontal region which might be ill-defined by slow-roving meanders and eddies

in the circulation. This mixing region could be delineated by a plot of the sea surface isotherms. The movement of these disturbances could be tracked by successive sampling of the surface isotherms. These were the factors that augured for the use of aerial sea surface temperature survey techniques.

Since it was known that equatorial water was both inshore of and beneath the California Current, the boundary between the two water masses must leave the surface and increase in depth as one headed west from the coast. This implies a general negative slope or increase in depth in the mixing layer as one proceeds but into the southbound water. In addition to the perturbations in the acoustic field introduced by the vertical structure of the meanders and eddies in the circulation, temporal and spatial changes were expected from other causes. In the subsurface boundary region between the north and southbound water masses, internal waves (Helmholtz) can exist. Also, internal waves propagating onshore from distant generating areas can be expected. More important, due to the proximity of the test area to the continental slope, internal waves generated by tidal forces over the slope can be expected. It is interesting to consider that the propagation directions of some of these waves would be normal to each other, implying a spiked field analogous to crossing seas.

One of the functions of the surface ship was to delineate the test area. The requirement was to find an acoustically reliable area for the experiment that the submarines could reach and return from, as well as complete the tests, within the allotted time. Additionally, the area was to be within surface ship range. In general terms, it was a problem of determining the location of the intersection of four sets of conditions: operating conditions on two submarines and one surface ship, and sonar conditions in the environment. Bathythermographs on file at the National Oceanographic Data Center were reviewed and it was concluded that the area approximately 100 miles due west of Point Arguello was optimal to search for the exact test site. It had been planned to locate the exact test site, radio in the coordinates, proceed with equipment checkout, and then initiate the intensive environmental survey. B.T.'s # 103 through # 112 are the results of the test site location program (see Figure 2-1).

B.T. # 103 is located southeast of Rodriguez Dome in 750 fathoms of water. When compared with the rest of the run, and especially B.T. # 104 on the other side of Kodriguez Dome, it may be indicative of upwelling caused by strong (NNE, 22 kts) offshore winds.

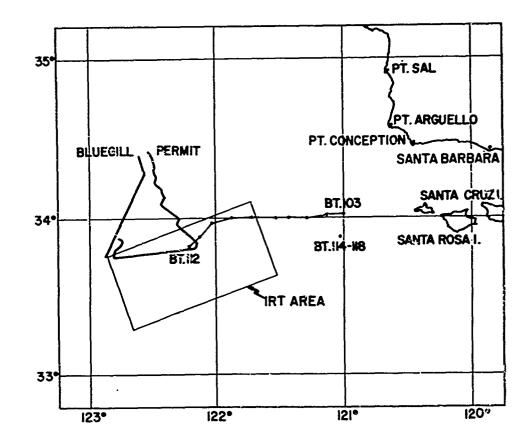


Figure 2-1 Location of Experiment

B.T.'s # 104 through # 108 show a surface layer 150 to 200 feet thick and at least 1°F warmer than the layer to the east (B.T. # 103) or to the west (B.T. # 110 through 112). This may be indicative of a warm tongue of north-bound equatorial water (Figure 2-2).

B.T. # 109 shows a slightly negative gradient in the surface layer. This is indicative of a frontal or transition region, and, when compared to B.T.'s # 104 through # 108 and # 110 through # 112, can be construed to be in the transition region between northbound and southbound water. (See infrared thermometer survey discussion for further analysis of this region.)

B.T.'s # 110 through # 112 show a surface layer of colder water 190 to 230 feet thick. It was assumed that the southbound water mass exhibiting good sonar characteristics had been reached, and test site coordinates were radioed in to San Diego at the completion of B.T. # 112.

A plot of layer depth, as read from B.T. # 104 through # 112, versus distance, measured from the location of B.T. # 104 (Figure 2-3), can be fitted with the following linear regression line:

z = 159 + 0.82 x

where:

z = layer depth in feet

x = distance in nautical miles from 34° 01'N, 121° 08'W (location of B.T. # 104) in a westerly direction

This indicates a general increase in layer depth proceeding west from the continental shelf break. Superimposed on the sloping linear regression line, representing the mean layer depth, is an apparent trigonometric variation of layer depth. This variation appears to be a cosine wave with a slight phase shift, as zero phase would be a few miles east of the location of B.T. # 104. The height of this wave is 50 feet and its length 36 miles (58 km). More detailed analysis of this waveform indicates that it does not represent internal waves, but rather is a result of the water mass circulation and upwelling due to wind. Specifically, the rise in the mixed layer toward an apparent crest when approaching the location of B.T. # 104 from the west appears to be due to northerly winds and the concomitant wind drift upwelling. Additionally, the rise in the mixed layer towards a crest in the vicinity of B.T. # 108 appears due to sampling in the transition zone or front between the warmer and cooler water referred to before. So it may be said that the waveform of the mixed layer depth versus distance plot is an apparent wave and has little to do with internal waves.

In Figure 2-3, it appears that the thermocline can be adequately described by the bundle of isotherms contained within the $53^{\rm O}$ to $55^{\rm O}$ F range, so that the $55^{\rm O}$ F isotherm was assumed to be representative. It is of interest to note that Emery and Summers¹ chose the $55^{\rm O}$ F isotherm as the thermocline indicator in their work of March and August 1961. They noted variations of up to 90 feet in isotherm depth. The plot of $55^{\rm O}$ F isotherm depth versus distance can be fitted with the following linear regression line (Figure 2-3):

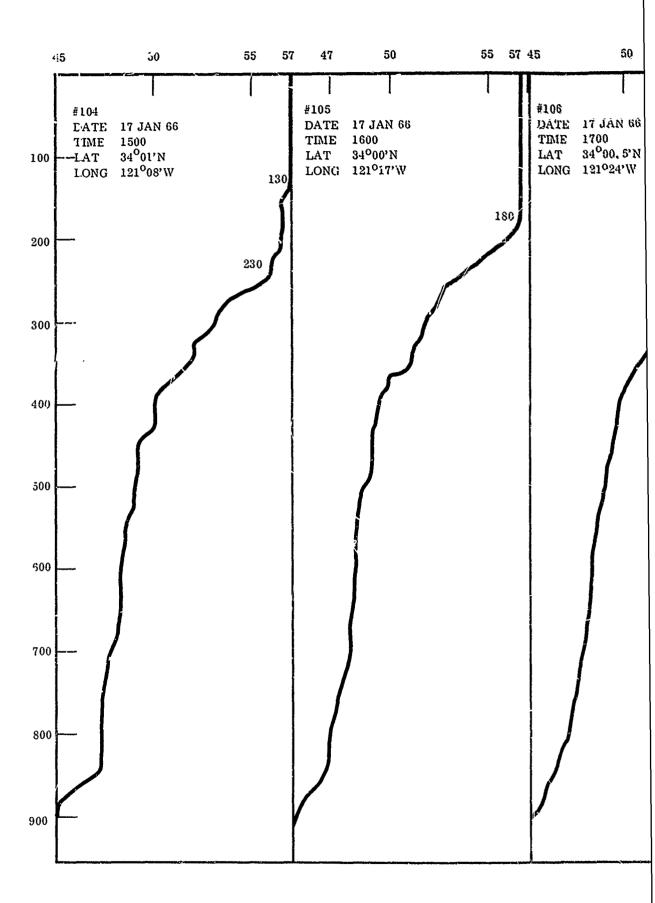
z = 242 - 0.49 x

where:

 $z = 55^{\circ}F$ isotherm depth in feet (thermocline)

x = distance in nautical miles from 34° 01'N, 121° 08''V is a westerly direction

This indicates a gradual decrease in the depth of the thermocline as opposed to the increase in the depth of the mixed layer over this same interval. Superimposed on this sloping linear regression line, representing the mean depth of the



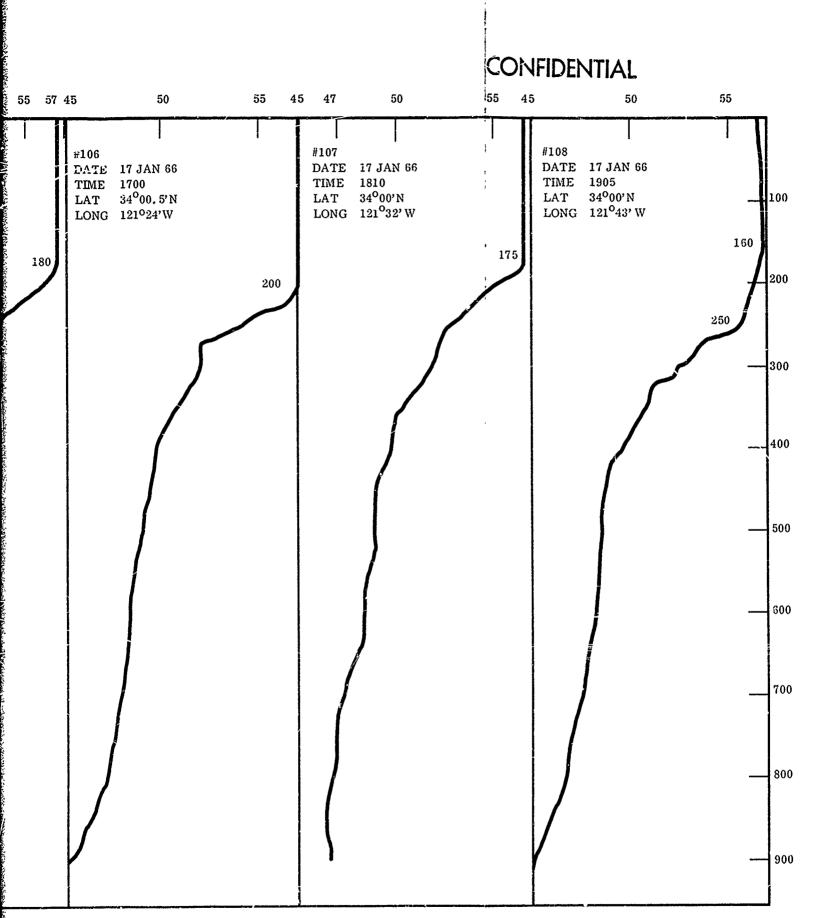
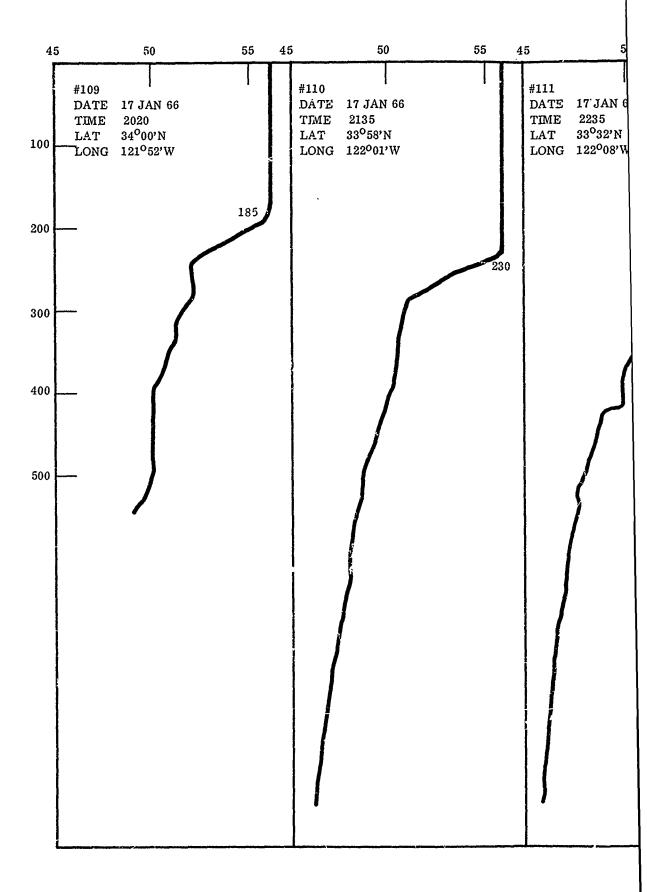


Figure 2-2a B.T.'s #104 through #108





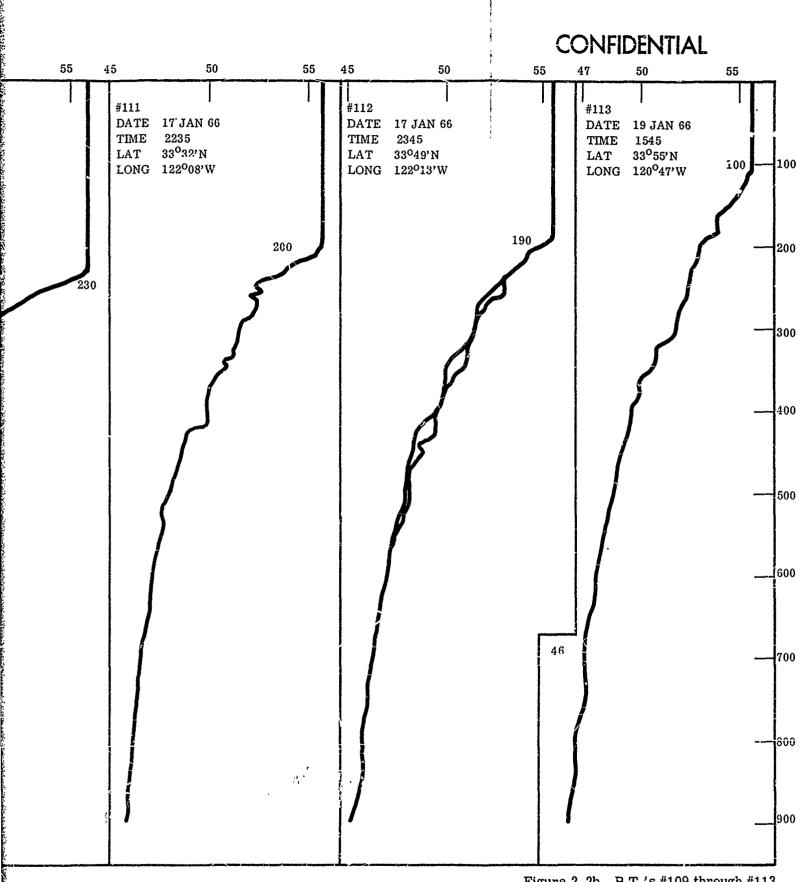


Figure 2-2b B.T.'s #109 through #113



thermocline, is a different apparent periodic variation of the thermocline depth. This variation appears to be a phase-shifted cosine wave or possibly a sum of cosine waves. The wave height is of the same order as the apparent mixed layer wave height, namely about the late.

The wavelength is deemed to be spurious in any application to internal waves as it is probably forced by the sampling interval in the B.T. run. The variations in depth of this isotherm are, however, taken to be real. It should be noted that only B.T. # 104 and # 108 cause the discrepancy between apparent wavelengths of the mixed layer and thermocline.

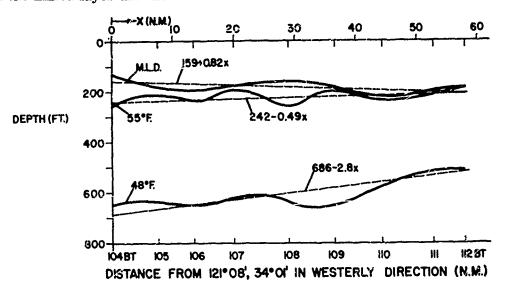


Figure 2-3 Thermal Structure

The $48^{\rm O}F$ isotherm depth has been plotted in Figure 2-3 and can be compared to the $55^{\rm O}F$ isotherm. The following linear regression line describes the mean depth of the $48^{\rm O}F$ isotherm:

z = 686 + 2.8xwhere: $z = 48^{O}F \text{ isotherm depth in feet}$ $x = \text{distance in nautical miles from } 34^{O} \text{ Ol'N,}$ $121^{O} 08'W \text{ (B.T. } # 104) \text{ in a westerly direction}$

This indicates a decrease in the mean depth of the isotherm proceeding west in the sampling area. It is noted also that this slope is five times as great as the 55°F isotherm (2.8 vs. 0.49). As was mentioned previously, the general circulation has been well studied in this area. Northbound water of equatorial origin has been determined to flow beneath the generally southbound California Current. If the assumptions are made that the slope of the isotherms at this depth are indicative of the slope of the isopycnals and the fields of mass and pressure are in mutual adjustment, then the isobars tend to slope down from

east to west resulting in a northbound current at these depths. Although this conclusion is based on speculation, it does agree with what has been measured.

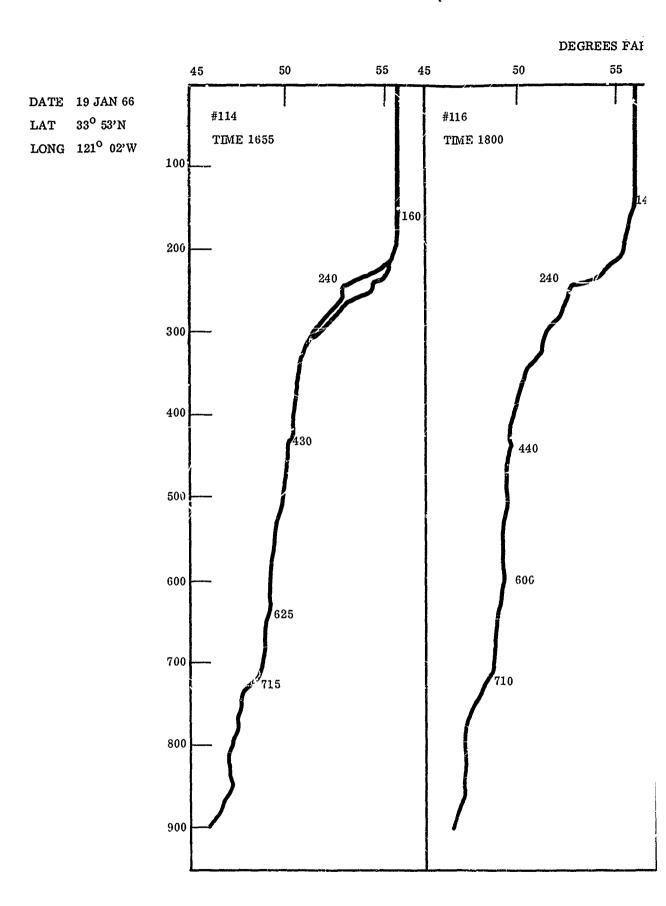
Unfortunately, the lack of data on the slope of the isohalines precludes a stronger analysis. Under the assumptions, however, the increased slope of the isotherms with depth is expected. This again points up the need for data and knowledge of the oceanography of a region so as to be able to predict, albeit in gross terms, the structure of the acoustic field.

Four hourly B.T.'s (# 114 through # 118) were taken on January 19, 1966 at 33°53'N, 121°02'W (Figure 2-4). The total excursion of the mixed layer depth was 60 feet, from 140 feet to 200 feet in depth. The mixed layer temperature increased by 0.5°F during this time. B.T. # 118 shows a slight inversion in the surface layer, which may be due to radiative cooling. The 55.5°F isotherm increased in depth from 180 feet to 232 feet, or a 52-foot excursion. The warming of the surface layer in this manner, during the time 16:55 to 20:10, indicates an intrusion of warmer water with its leading edge at the surface. Rather than due to internal waves alone, it appears that a meander in the circulation passed into the test area or, possibly, the incursion was due to the tidal advection of warmer, inshore water.

Although the bathythermograph run was completed two days before the first infrared radiation thermometer (IRT) flight and four days before the flight on which good data was taken, the B.T.'s tie in with the IRT data and the sound velocity profiles (SVP) taken by PERMIT. The picture that unfolds when interpreting the data, as limited as it is, from these three sources reveals a complexity in the environment that implies the necessity of refined environmental sampling in any acoustic experiment.

Three IRT runs were scheduled, one of which was to be at night to document the day-night effect. The sampling track was set up such that the longer sampling legs were normal (northeast-southwest) to the coastline with shorter interconnecting legs running parallel (northwest-southeast) to the coast. The sampling pattern was designed this way on the assumption that the general orientation of the sea surface isotherms would be parallel to the coast, with colder water off-shore. This assumption was based on the known circulation of the California-Davidson Currents system and verified by researchers on the West Coast.

As can be seen from Figure 2-5, the isotherm pattern existing at the time of the tests was far more complicated. Figure 2-5 shows a pincerlike formation of cold water in the top (northwest) section of the 30- by 60-mile wide survey area and warmer water in the bottom (southeast) section. This anomalous situation was noted by the Tiburon Marine Laboratory (BCF) and a week earlier by the Fisheries Research Board (Canada) personnel. As was mentioned previously,



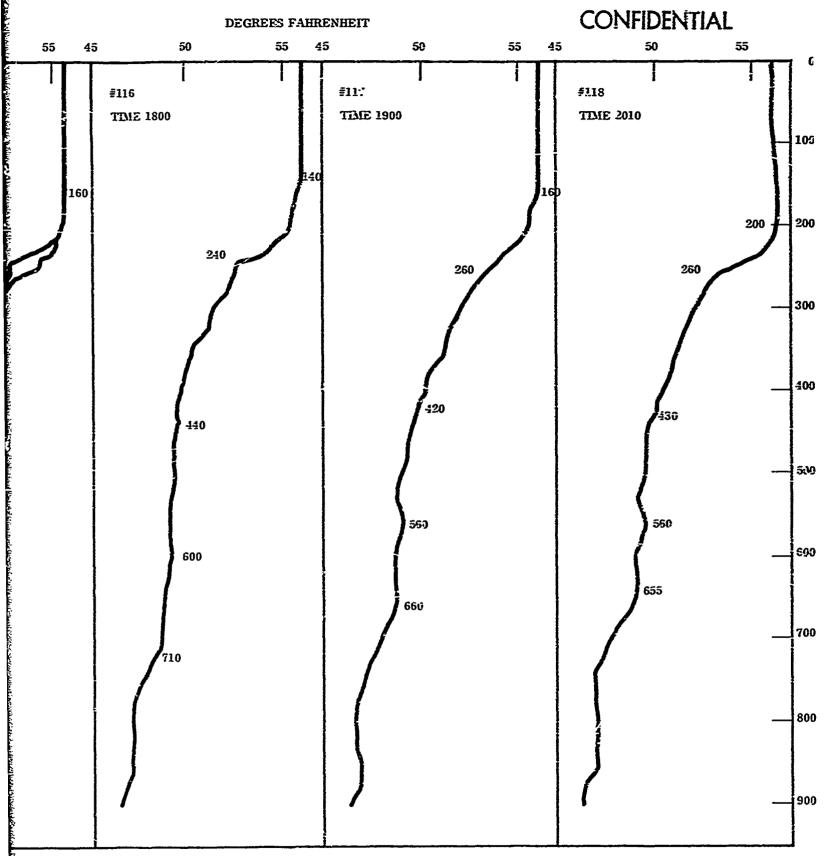


Figure 2-4 B.T.'s #114 through #118

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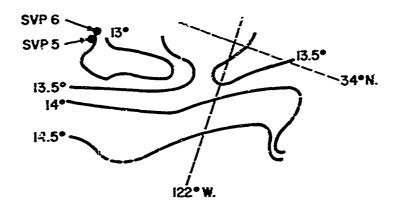


Figure 2-5 Isotherm Field At the Time of Test

the isotherms were expected to be running generally northwest to southeast, but, as is evident from this plot, they are generally running northeast-southwest. This indicates a renewed flux of cold water from the north or a meander in the circulation. This plot was one of three based on a good trace, or one in which the noise level was low. Some information is available from the previous runs and can be tied into this plot to indicate a time history of the circulation pattern over these three days (Figure 2-6).

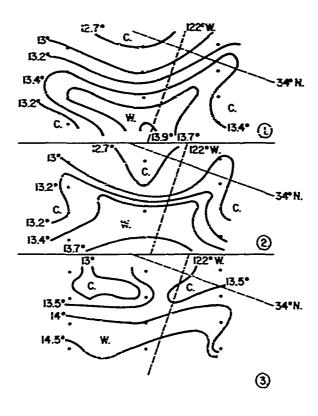


Figure 2-6 Three-Day Surface Temperature (Airborne IR) Pattern

The IRT run on January 19, 1966 from 1401 to 1557 hours shows a general east-west orientation to the isotherms, slightly concave northwards, showing a gradual influx of cold water from the north into the survey area. There is also indication of warmer water pushing southwest on the east side of the survey area.

The IRT run on January 20, 1966 from 0509 to 0656 hours shows a gradual destruction of the east-west orientation of the isotherms, especially on the north side of the survey area. The influx of colder water from the north is becoming more apparent as the concavity of the isotherms to the north is increasing. On the west side of the survey area another influx, or pincer, of colder water is apparent. On the east side, the intrusion of warmer water to the northeast has abated, as the temperatures in this tongue have dropped somewhat. It may be that this was not warm water pushing northeast and cooler water pushing southwest, but only the latter. This inference seems strengthened by the general temperature decrease in the southeast part of the survey area and the increase in the temperature gradient in this region coupled with the decrease in the gradient in the northeast part of the area.

The first two runs, although composed of noisy data, do show a flow of cold water from the north and pincers of cold water coming in from the sides of the survey area. It is interesting to note the change in location of the most southerly part of the 12°C isotherm. In the thirteen hours from run one to two, it had moved ten miles or at an average velocity of 0.75 knots.

The third IRT run, on January 21, 1966 (#3) from 1022 to 1213 hours, shows the complete destruction of the previous orientation of the isotherms on the northern side of the area. It appears that the influx of cold water on the northern side has abated while the pincer movement of colder water from the sides has intensified. The southern side of the area has regained the east-west orientation of isotherms.

The net effect of what has happened over the three-day period is that cold water has moved in from the north and, in a pincer-like movement, detached a portion of the warmer water.

In attempting to integrate the IRT and B.T. data, it should be noted that B.T. # 112 was taken on January 17 at 2345 while the first IRT run was on January 19 at 1500. As a result, one must assume that the general structure of the sea surface isotherms in evidence on the first IRT run was existent during the B.T. run. On this assumption, it then appears that although the B.T. run did pass from warmer water to colder, the end of the run was through an eddy or meander rather than a well-defined water mass boundary oriented northwest to southeast. Since the vertical stratification varies when sampling through a warm intrusion or a cold pincer formation, as noted, isotherms will also vary in depth during the sampling run. This variation in isotherms' depth is a

result of the stratification associated with meanders as well as internal waves present in the area (Figures 2-7 and 2-8).

Experience gained during this exercise indicates that future IRT sampling programs should be of two distinct types. The first type of IRT sampling program should be on a large scale, both before and after the tests. This type of sampling would yield information on the gross changes in the environment during the tests. The second type should be on the scale of the tests and the flight tracks should be closely spaced. This type of sampling would yield data on the fine structure of the test area and would be integrated with thermistor and/or bathythermograph data.

The sound velocity profiles (Figure 2-9), seven in number, taken by the PERMIT have been adjusted to account for separation of approximately 30 feet between the pressure transducer and the velocimeter. The range of mixed layer depth varies from 100 feet (SVP # 5) to 240 feet (SVP # 7), and the mean depth is 194 feet. This compares well with a mean layer depth of 190 feet from the bathythermograph data. SVP's #2 and 3 were about two nautical miles apart in space and two hours apart in time. The surface layer sound velocity value did not change but the layer depth increased by 20 feet, from 180 to 200 feet. Of more interest is a comparison of SVP's #5 and #6, taken some 18 hours after #2 and #3, and about 20 miles away. SVP's #5 and #6 (Figure 2-10) are about two miles apart in space and one hour in time. The mixed layer depth increased from 100 feet to 210 feet, an excursion of 110 feet, during this sampling interval. The surface layer velocity did not change nor did the velocity at 470 feet. In addition, there is a slight positive velocity gradient or bump in both profiles at about 420 feet. Therefore, it is concluded that the measurement is real and not due to instrumental error.

The maximum change in velocity occurred at a depth of 210 feet and was 25 feet per second. Assuming a constant salinity, the temperature must have changed by 4°F at that depth during the sampling interval to bring about this velocity change. This temperature change at constant depth is the greatest measured, although the change at 240 feet from B.T. # 109 to # 110 was 3°F. An evaluation of horizontal temperature gradients between the SVP's and B.T.'s cannot be made because of the differing sampling intervals. The third IRT run over the area was completed about five hours after SVP's #5 and #6 were taken. The cold tongue, or pincer, on the northwest side of the survey area, as noted previously, extended through the area of SVP's #5 and #6. If the variation in layer depth was not caused by internal waves, it may well be that the sampling interval extended over the leading edge, or a cold wedge, of the intrusion. If, on the other hand, the sampling interval extended through a meander from an upwelling to a sinking region, the mixed layer would exhibit this change also.

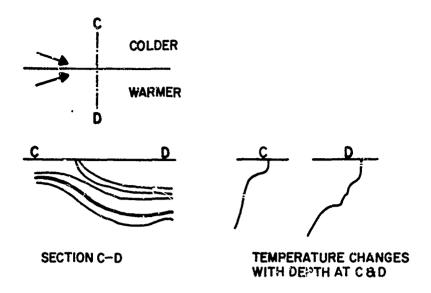


Figure 2-7 Structural Models of Convergences

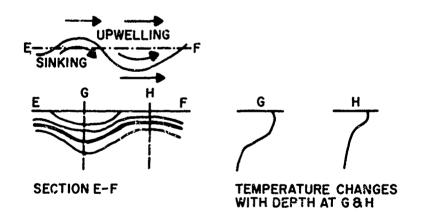
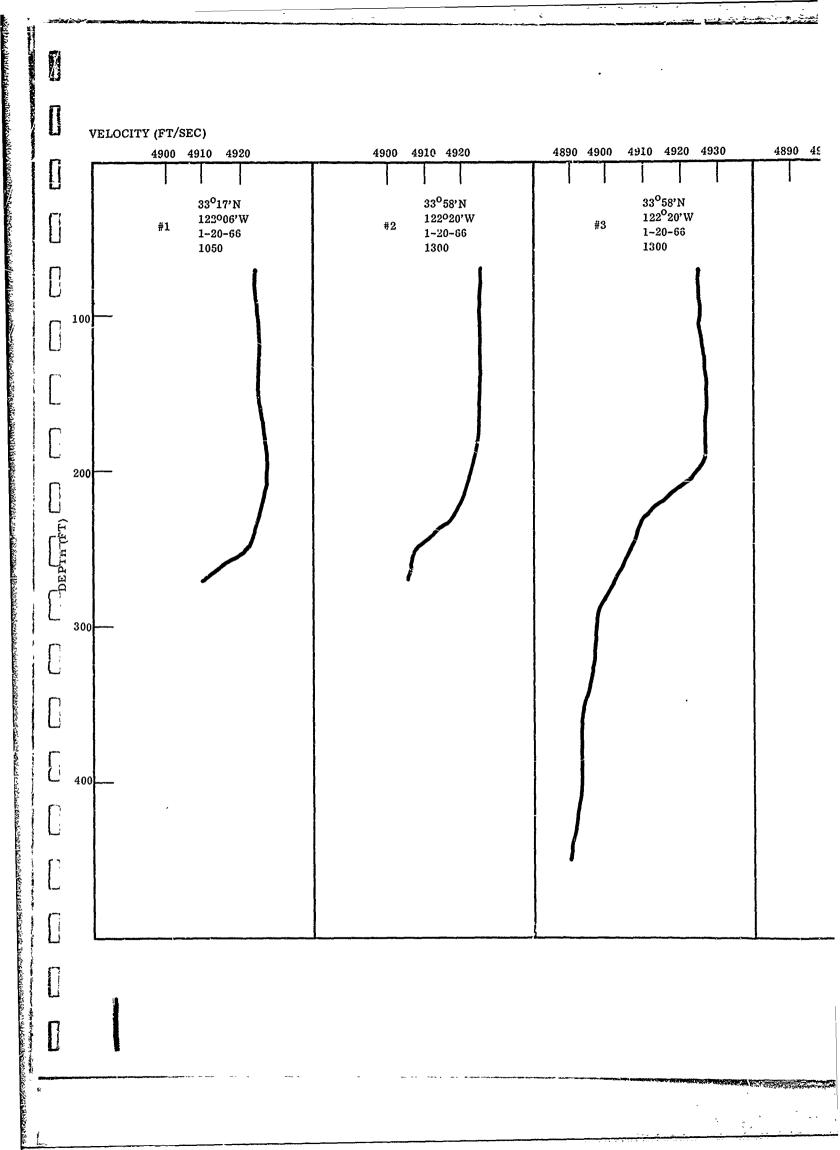


Figure 2-8 Upwelling and Sinking at a Meandering Boundary



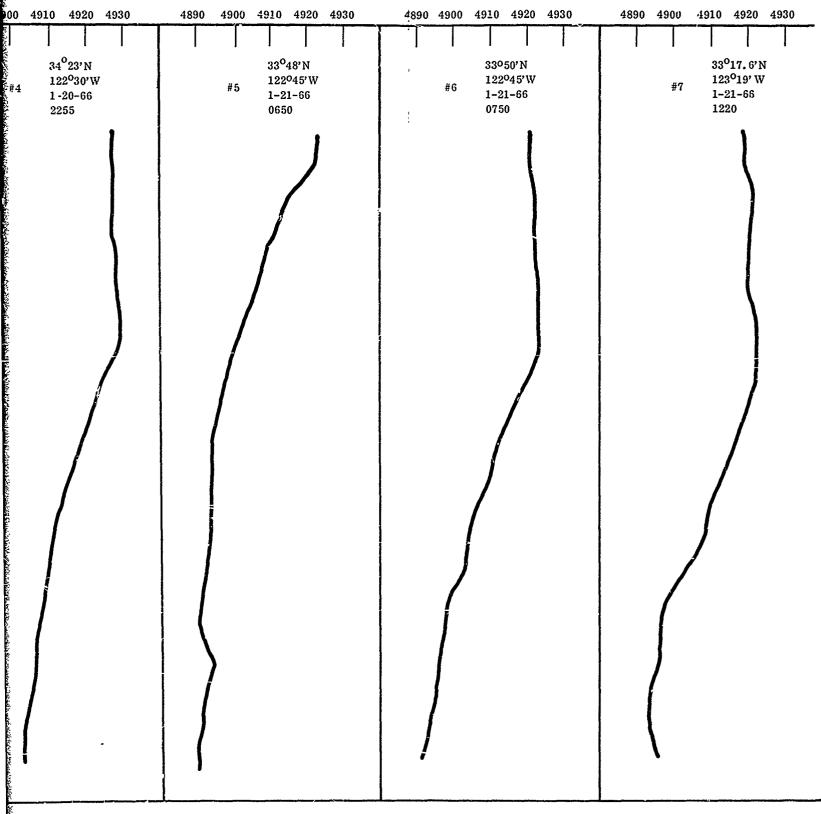


Figure 2-9 SVP's From USS PERMIT

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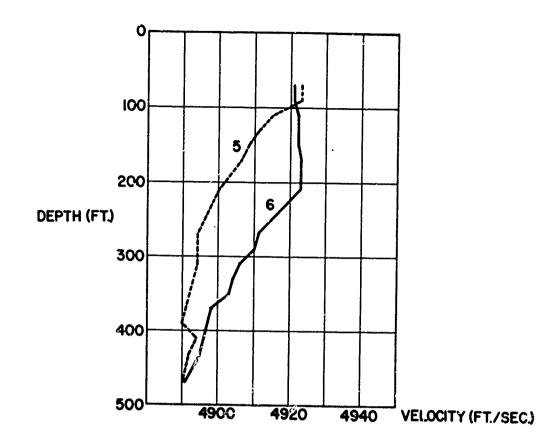


Figure 2-10 Comparison of SVP's 5 and 6

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EFFECTS OF ENVIRONMENT ON ACOUSTIC TRANSMISSION

The purpose of the submarine tests involving the USS PERMIT and the USS BLUEGILL was to measure various transmission parameters, in particular signal-to-noise ratio (S/N). At the time of the experiment, a surface channel existed whose depth was approximately 200 feet, as determined from SVP's taken during the test, although this varied from a maximum of 240 feet to a minimum of 140 feet. Data was taken with the BQS-6 sonar in both active and passive modes. The results were compared to predictions made by a ray trace program and good agreement was obtained.

SINGLE-FREQUENCY MEASUREMENTS (ACTIVE SONAR)

Recordings of one-way transmission of active sonar signals from the USS PERMIT, as received on the USS BLUEGILL, were made with both ships moving at constant speed, on parallel courses, and at ranges of 5400 and 10,000 yards (Figure 3-1). Both ships were in the surface channel with the PERMIT at a depth of 165 feet and the BLUEGILL snorkeling at a depth of

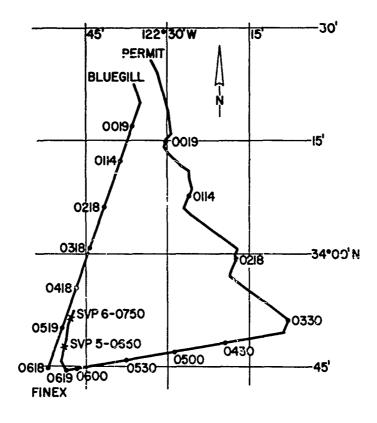


Figure 3-1 Track Chart for Run 2

TABLE 3-1
SUMMARY OF TEST CONDITIONS

Run #	Leg #	Nominal Range (yds)	Actual Ra	nge (yds) ¹	Depth ²
II-1	1	5K	4680E	ATF	165
	2	10K	9500	ATF	165
5	3	20K	23500E		165
knots	4	40K	41000	-	165
	5	60K	56350	ATF	165
П-2	1	5K	5430E	ATF	165
	2(Note course	10K	10350	ATF	165
	change during				
	passive run)				
5	3	20K	21300	-	180
knots	4	40K	40000	ATF	150
	5	60K	60000	-	150
II-3	1	5K	5000	ATF	150
	2	10K	9900	\mathtt{ATF}	150
8	3	20K	20000	ATF	150
knots	4	40K	40000	\mathtt{ATF}	120
	5	60K	59500	-	120

Test instrumentation located on board the BLUEGILL consisted of a two-channel Ampex A.M. (direct) tape recorder. One channel was used to record the signal received by a single hydrophone of the BLUEGILL's sonar array; the other channel was used as a voice channel.

Where range is followed by \underline{B} or \underline{E} , sonar range at beginning or end of run is indicated. Otherwise, range is estimated.

²Depth refers to tracking ship keel depth. Center of BQS-6 sphere is approximately 15 feet less. Target keel depth equals approximately 55 to 60 feet for all runs.

⁶⁰ feet. The sonar signals consisted of 150 msec pulses at a frequency of 3.5 KHz. Operating conditions are specified in Table 3-1.

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Test instrumentation on board the PERMIT (source ship) consisted of a 14-channel Precision Instrument F.M. tape recorder. Three of the channels were used to monitor a single MASSA hydrophone located on the sail 50 feet from the center of the BQS-6 sphere. The three channels recorded the same signal at three different amplifications in order to extend the dynamic range of the recording system. A fourth channel was used as a voice channel and the other ten were used to record signals unrelated to this experiment. Approximately 6-1/2 minutes of data were collected at each range.

Upon return to the laboratory, the signals recorded on both ships were played back, using the same machines on which they were recorded, and processed using a TR-48 analog computer. A block diagram of the computer program is shown in Figure 3-2. As indicated in Figure 3-2, the signals were processed to obtain the power envelope, the sum of the areas of all power envelopes, and the sum of the areas of the log of each power envelope. Each of these quantities was recorded on a Sanborn strip chart recorder. The peak amplitudes of the power envelope and log of the power envelope of each ping, i.e., instantaneous peak power, received on the BLUEGILL were read from the strip chart and used to calculate the mean and variance of the received signal (Figure 3-3). A similar calculation was made for the pings received by the MASSA hydrophone located on the PERMIT. This gave a measure of the variance of the transmitted signal. In addition to calculating the mean instantaneous peak power of the signals received on the BLUEGILL, the mean power of each ping was calculated by dividing the sum of power contained in all pings by the number of pings times the length of each ping. This was done for both the actual power and the log of the power in order to convert the power to dbv.

The analysis of the signals as received on the BLUEGILL is summarized in Figure 3-4.

The variance at 5400 yards is four times greater than that at 10,000 yards, while at the same time the mean power is 2 dbv less, or about 63% of the mean power at 10,000 yards. A similar analysis of the signals received by the MASSA hydrophone located on the PERMIT indicated that the signal level was constant to within ± 0.05 dbv of the mean value for all pings (both 5400- and 10,000-yard ranges). Since the transmitted signal was constant, it is apparent that the variation in the received signal was introduced by the environment. (A direct comparison of the power received on the BLUEGILL and the power transmitted by the PERMIT is not possible because of the different recording techniques and hydrophones used.)

WIDEBAND MEASUREMENTS (PASSIVE SONAR)

The test geometry for the wideband measurements was identical with that used for the single-frequency measurements. The two ships were moving on parallel courses at constant speed (five knots) at each of the two ranges. The wideband

noise source was simply a snorkeling submarine (BLUEGILL) and the receiver consisted of the passive section of the BQS-6 sonar aboard the PERMIT. The received signal was filtered for the 1-2 KHz band.

Instrumentation for the wideband measurements was located entirely on board the PERMIT. It consisted of two TR-10 analog computers and the SUBIC At-Sea DDP-24 digital computer and associated peripheral equipment. The analog computers were used to obtain the signal-to-noise ratio because a recording of the received signal alone would be difficult to obtain due to masking by the ambient noise field.

The analog computers accepted signals from the right half and left half of the BDI loop of the BQS-6 sonar set, processed them, and fed them to the digital computer where the analog-processed signals were further processed to obtain signal-to-noise ratio. The digital computer also accepted information from the ship's sensors, such as target bearing, course, and speed (Figure 3-5). All of this information was averaged for about 2.5 seconds, and the average value of each quantity during this time was punched on paper tape. Approximately 20 minutes of data were taken at each range.

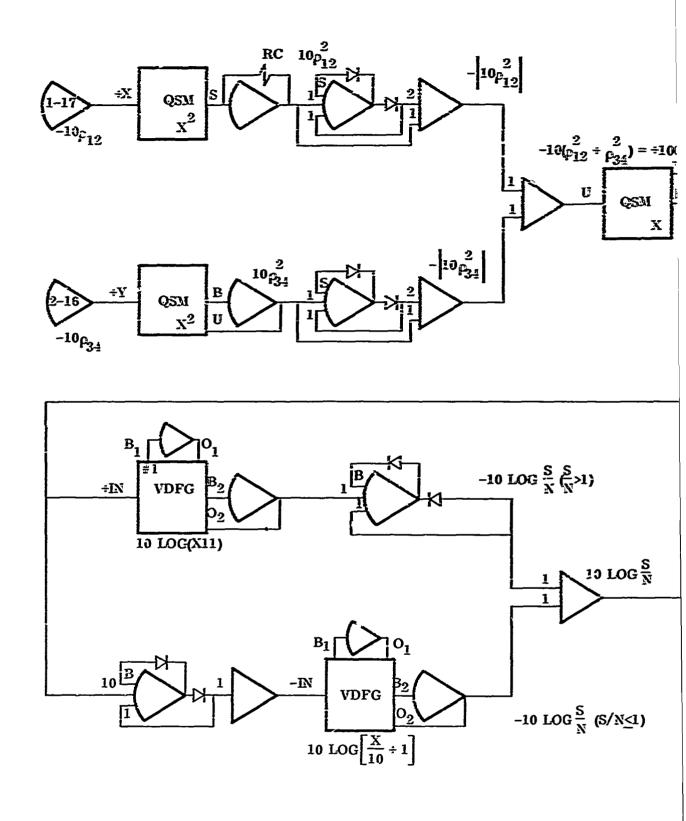
Upon return to the laboratory, the data tapes were printed in hard copy by the computer's typewriter. In addition, the mean, variance, autocorrelation functions for different lag times, and power spectrum of each of the recorded quantities was computed by the DDP-24 (see Section IV). A summary of the mean and variance of the signal-to-noise data is given in Figure 3-4.

At each range during the wideband noise measurements the BLUEGILL (noise source) was moving at constant speed, depth, and course and maintained the same position in relation to the PERMIT. During this portion of the experiment the BQS-6 sonar was in ATF mode. The PERMIT was also moving at constant course, speed and depth. Therefore, it may be reasonably assumed that the self-noise of each of the submarines, and the directivity index of the BLUEGILL relative to the PERMIT, remained constant during the experiment and that all variations in the signal (and, hence, signal-to-noise) were introduced by the environment.

COMPARISON OF WIDEBAND AND SINGLE-FREQUENCY MEASUREMENTS WITH RAY TRACE PREDICTIONS

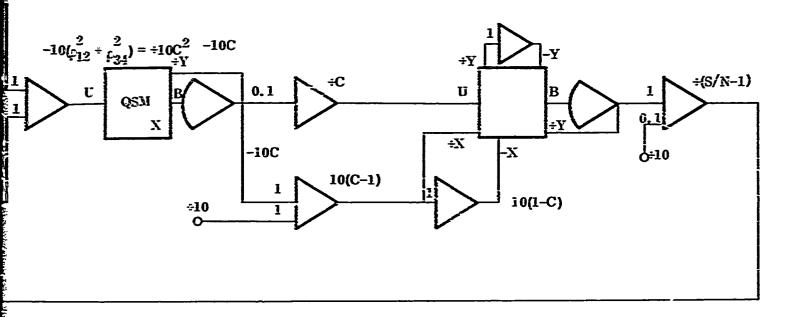
Description of Operational Ray Trace Program Through Internal Wave Fields

The ray trace program used for propagation loss computations can consider a particular class of sound velocity profiles which vary with range as well as depth. The class of variations includes a model of the perturbations to the



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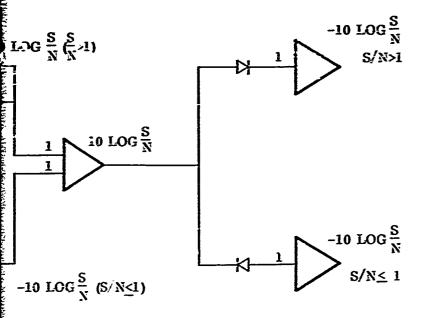


Figure 3-2 TR-48 Computer Program for S/N



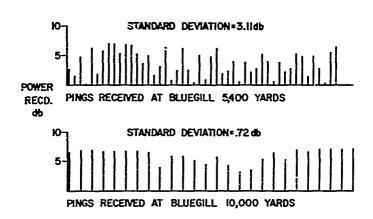


Figure 3-3 Time Series Record of Pings Received at BLUEGILL

			ACTIVE	PASSIVE
5 A V	YARDS	VARIANCE	6.22 (db) ²	6.62 (db) ²
J.4 K	IARUS	<u>MEAN</u>	5.91 db	-4.47 db
וח צ	YARDS	VAR!ANCE	1.44 (db) ²	-5.85 (db) ²
IO K	IMIDS	MEAN	7.84 db	-5.47 db

Figure 3-4 Comparison of Active and Passive One-Way Transmission Loss Data

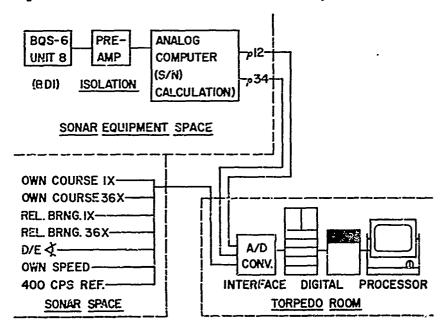


Figure 3-5 PERMIT Installation Block Diagram

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profile normally associated with the presence of internal waves in the thermocline. The usual ray tracing program traces a ray through layers of constant sound velocity gradient. As a layer is defined by parallel lines, the velocity profile is implied to be stationary over the range of interest. This is a convenient oversimplification and one which, in the region of a thermocline particularly, is often incorrect. The existence of an internal wave field in the region of the thermocline, a phenomenon which has been repeatedly documented directly by thermister chain measurements and indirectly suggested by acoustic measurements, disturbs the layer representation. The extension to ray trace being discussed purports to model this range dependent disturbance after the layer model.

Operationally, we will define the thermocline as a region of relatively sharply decreasing temperature. In many areas of interest in the ocean this occurs once or twice within a thousand or so feet of the surface; termed the permanent and the seasonal thermocline, these regions are capable of sustaining complex (water) wave motions called internal waves. As a result of this internal disturbance, a systematic change in sound velocity with range is set up which is, however, strongly confined to the strata defined by the thermoclines.

A simplified model of this variation was suggested by Lee^{2, 3} when he considered the stratum of a thermocline to be a sinusoidally bounded region of constant sound velocity gradient (Figure 3-6). We have adopted this technique with the exception that the program can easily be extended to consider a sum of sinusoids to represent the boundaries, that is, a finite Fourier representation can be made of any periodic boundary. The final model will then consist of N "layers," each with its own velocity gradient. N-3 of these are layers in the full sense of the word. The two layers bounding the thermocline have only one boundary parallel to the surface and the last, the thermocline, has prescribed periodic boundaries. By necessity, given the N gradients and one boundary of the thermocline, the second boundary is not arbitrary. Instead, it is calculated by fulfilling the condition that at some depth below the thermocline, the medium, and therefore the sound velocity profile, is undisturbed.

To trace through the thermoeline we have to return to the basic eikonal equations, as the literature is concerned almost entirely with layered media. The basis of calculations using a single velocity profile at all ranges, the ray constant, is no longer valid. On the other hand, the internal wave field in the thermoeline is quantitatively only responsible for a perturbation on the ray paths and, therefore, the trajectory can still be thought of (to a good approximation) as continuous circular arcs. The radius of curvature at each point in space, directly derived from the eikonal equations, assuming cylindrical symmetry, is:

$$\frac{d\theta}{ds} = \sin\theta \frac{\partial c}{\partial r} - \cos\theta \frac{\partial c}{\partial z},$$

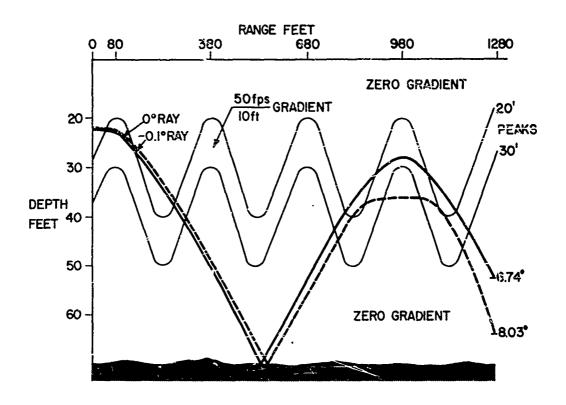


Figure 3-6 Model of Internal Wave

where θ is the angle the ray makes to the horizontal at the point (r, z), c is the speed of sound at that point, and s is the arc length along the ray to that point. By taking finite arc steps and calculating a new curvature at the end of each step, a differential approximation to the exact trajectory is achieved. The resulting program has been found to yield results numerically equivalent to Lee's study despite the fact that he used a very different approach to trace the rays and then an independent method of calculating energy.

The perturbation to the ray paths can be visualized as follows: the effect of a region of negative gradient is to bend rays towards the minimum velocity. The rate of bending (curvature) depends on the amplitude of the vector product $\frac{d\mathbf{r}}{ds} \times \nabla \mathbf{c}$, and the amount of bending brings into consideration the total are length required to pass through the region. In the case of an undisturbed layer, grad \mathbf{c} is always downward and the grazing angle to the layer, $\frac{d\mathbf{x}}{ds}$, which is a monotonic function over a range of adjacent rays, requires that both the rate and the amount of bending will be monotonic over such a range. When the layer is disturbed, the direction of $\nabla \mathbf{c}$ varies so that the local grazing angle and the arc length to pass

through the region are no longer a function of $\frac{dx}{ds}$ alone, and the range of incoming rays over which monotonic bending applies is restricted by the scale of the disturbance. Over a characteristic wavelength of the disturbance, differential bending can occur for bundles of adjacent rays. This convergence and divergence of ray paths will result in corresponding changes in the sound intensity beyond the disturbed layer.

The ray trace program described above was used in an attempt to predict transmission loss and signal variance at the ranges of interest (5400 and 10, 000 yards). The SVP taken immediately prior to the 5400-yard measurement (SVP #4) was used as a base, with a sinusoidal perturbation inserted having an amplitude of 50 feet, based on results of the environmental survey, and a mean depth of 200 feet. The source was placed at 50 feet, corresponding to the depth of the BLUEGILI. Energy was calculated at 100-yard intervals at a depth of 150 feet, corresponding to the depth of the PERMIT.

Wavelengths (for internal waves) of 3000, 5000, and 9000 yards were chosen from the results of the autocorrelation analysis. The average decay time (to zero) of the autocorrelation function of S/N is approximately 150 seconds at 5 knots. When this is translated to distance, a result of

150 sec x
$$\frac{5 \text{ N.M}}{1 \text{ hour}}$$
 x $\frac{1 \text{ hour}}{3600 \text{ sec}}$ x $\frac{2000 \text{ yds}}{1 \text{ N.M.}} = \frac{15000 \text{ yards}}{36} = 420 \text{ yards}$

is obtained. Recalling that the autocorrelation function of a sinusoid is another sinusoid of the same frequency, it is evident that the time required for such an autocorrelation function to decay to zero is equal to one-fourth the period (or one-fourth the wavelength). On the basis of the foregoing, the disturbance which caused the observed modulation of the S/N ratio and of the active signal must have dimensions of approximately 1700 yards. However, the disturbance is not a perfect sinusoid and, therefore, it is felt that this dimension simply represents the order of magnitude of the disturbance size.

The sinusoidal internal waves defined by the above parameters were moved past the sound source in 30° phase increments, yielding 12 values for energy at each range. These 12 values at the ranges of interest were then averaged to obtain the mean value of predicted transmission loss at that range, and also were used to obtain an estimate of the variance. The values of the mean and variances for each wavelength were plotted and may be found in Figures 3-7, 3-8, and 3-9. Figure 3-10 presents a summary of the predicted mean and variance of the transmission loss at the ranges of interest.

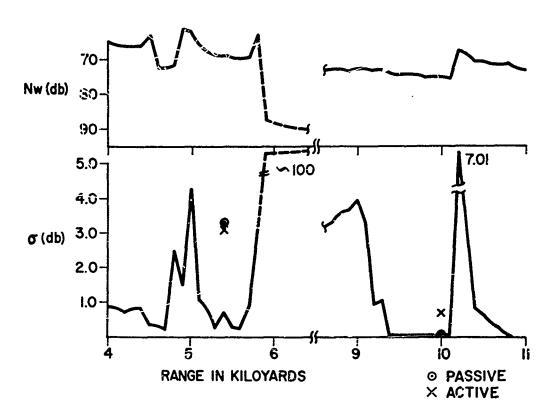


Figure 3-7 Predicted Nw and σ ($\lambda = 3K YDS$)

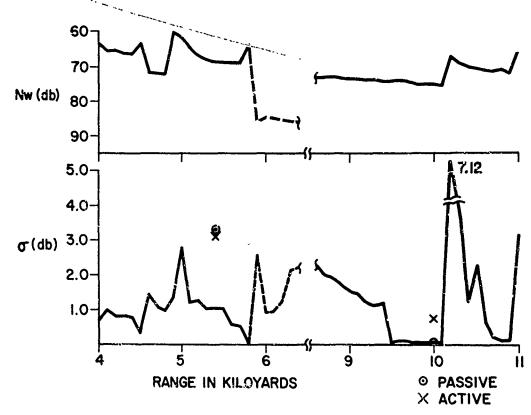
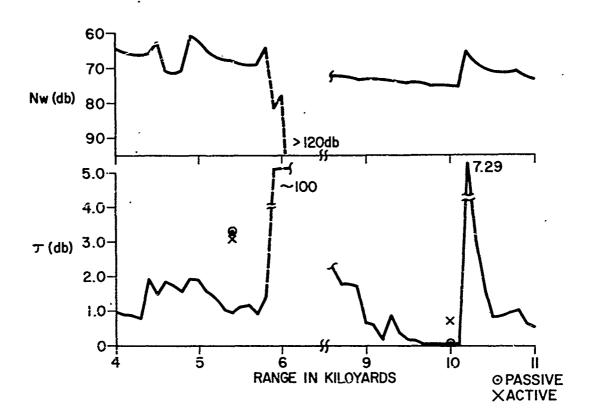


Figure 3-8 Predicted Nw and σ ($\lambda = 5K \text{ YDS}$)



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Workston I

Table 1

Figure 3-9 Predicted Nw and σ ($\lambda = 9K YDS$)

λ	RANGE	5.3K	5.4K	5.5K	9.9K	10.0K	10.1K
3K	MEAN (db)	68.68	68, 94	69.60	75.20	75.20	75. წ 0
	VAR.	0.06	2.48	0.09	0	0	0
5K	MEAN (db)	68.84	68.99	69.32	75.20	75.20	75.60
	VAR.	1.16	1.06	0.32	0	0	0
9K	MEAN (db)	65. 67	67.76	68. 67	75.20	75.20	75.20
	VAR.	1.29	0.95	1.17	0	0	0

Figure 3-10 Predicted mean and variance

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From Figures 3-7, 3-8, and 3-9, the mean and variance of the transmission loss are, in general, independent of the wavelengths of the internal wave chosen. Also, in the range 5300 to 5500 yards, there is a moderate variation predicted in the signal strength, whereas in the neighborhood of 10,000 yards, the variation predicted is zero. Referring to Figure 3-4, this prediction agrees favorably with results obtained for both the wideband and single-frequency measurements discussed in the preceding sections. It is emphasized that both ships were in the surface channel, i.e., above the internal waves, and there is still a noticeable effect on the signal strength.

The physical explanation for the higher variance at 5400 yards may perhaps be most easily seen by referring to Figure 3-11. This figure shows a simplified ray diagram, indicating the positions of the PERMIT at 5400 and 10,000 yards. The calculation was based on the sound velocity profile taken immediately before the 5400-yard test, and was done without any internal wave representation being included. It may be seen that, at a range of 5400 yards and a depth of 150 ±5 feet, the PERMIT was at the edge of the ensonified region. By contrast, at a range of 10,000 yards and a depth of 150 ±5 feet, the PERMIT was in the middle of the acoustic field. Under these conditions, a small disturbance to the depth of the thermocline would have a major effect on the acoustic energy at the 5400-yard range, while it would have a minor (if any) effect on the acoustic energy at 10,000 yards.

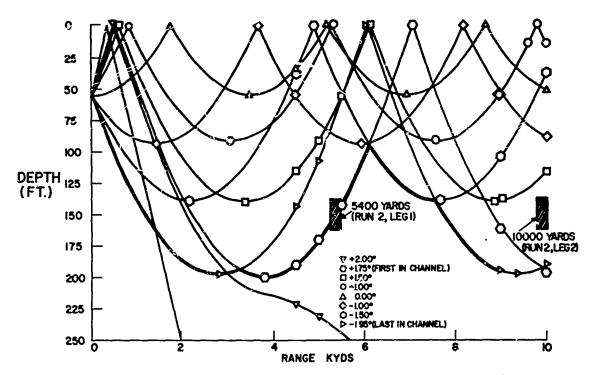


Figure 3-11 Position of PERMIT Relative to Predicted Acoustic Field, Run 2, Legs 1 and 2

It may be argued that the observed variance might also be due to the influence of surface fluctuations, causing the surface-reflected rays to deviate from specular reflection from an ideal flat surface. At the time of the test, surface conditions observed were 9- to 10-second swells. Therefore, it may be expected that this period would show up as a strong component in the S/N power spectrum if the surface were affecting the signal in the 1 to 2 KHz band. An estimation of the spectrum, calculated by the DDP-24 computer, does not show any peak in the 1 Hz region for either the 5400- or 10,000-yard ranges. It is therefore concluded that the surface fluctuations did not have an important effect in the 1 to 2 KHz band.

Referring again to Figure 3-4 for the wideband measurements, the mean value of energy at 10,000 yards dropped to about 63% of the value that it had at 5400 yards, or a drop of about 2 db. At the same time, the mean value of energy at 10,000 yards for the single-frequency measurements increased by about 2 db over the value at 5400 yards. These results, which at first may seem contradictory, are not inconsistent with the data.

If we let:

 S_1 = mean value of single-frequency signal at 5400 yards

 $\mathbf{S}_{2}^{}$ = mean value of single-frequency signal at 10000 yards

 \mathbf{S}_3 = mean value of wideband frequency signal at 5400 yards

 S_4 = mean value of wideband frequency signal at 10000 yards

 $N_1 = noise$ (broadband)

 N_2 = noise (single frequency)

C = amplification factor for single-frequency signals

We may now obtain the following independent equations.

$$\frac{S_3}{N_2} = 4.30 \tag{1}$$

$$\frac{S_4}{N_2} = 2.66$$
 (2)

$$(S_1 + N_1) = 3.90C$$
 (3)

$$(S_2 + N_1) = 6.00C$$
 (4)

It is evident that these are six unknowns (C is a parameter) and only four independent equations. In order to obtain unambiguous results, it is necessary to know either S $_3$ + N $_2$ and S $_4$ + N $_2$ or $\frac{S_1}{N_1}$ and $\frac{S_2}{N_1}$. This would yield six independent expressions from which it would be possible to determine all of the unknown quantities.

The present ray trace program considers the signal as a broadband one, treating all frequencies with equal weight. Referring to Figure 3-10, it is seen that the predicted result is a loss of about 7 db between the 5400-yard and the 10,000-yard ranges. This corresponds, qualitatively, to the experimental observations in the wideband case where there was a loss of about 2 db. The difference between the predicted and observed transmission loss for the single-frequency measurements may be explained by several different phenomena. First, phase interference at 5400 yards, phase reinforcement at 10,000 yards, or a combination of both may account for the discrepancy. Second, the assumption of a constant noise field at both ranges may not have been correct. This would also possibly account for the discrepancy in the magnitude of the predicted and observed transmission loss between the two ranges. There are, in addition, many other factors which may contribute to this difference, some of which may be completely unknown to us.

AUTOCORRELATION RESULTS

INTRODUCTION

Part of the analysis of the S/N data performed after returning to the laboratory consisted of obtaining the autocorrelation of the data about its least-square fit line as a function of lag time. This was done using the DDP-24 computer with a special data reduction program. This program displays the raw data (S/N, bearing, course, speed, or D/E angle) in blocks of up to 100 data points at one time. Sections of up to 1000 data points, on consecutive scope displays, may then be selected by the light pen for statistical analysis.

The statistical analysis section of the program computes the least-square fit, mean, and variance of the selected data. These quantities are then used to compute the autocorrelation about either the mean or the least-square fit line, which is then displayed on the scope. The values may then be printed by the typewriter, the power spectrum of the data may be computed and displayed (and printed, if desired), or the computer may be instructed to return to data inspection. All of these alternatives are selected by means of the light pen. Typical scope displays generated by this program are illustrated in Figures 4-1 through 4-7.

The form of the autocorrelation function about its mean suggests that it consists of two statistically unrelated components. Thus, for a stationary random function of time, f(t), which can be written as

$$f(t) = f_1(t) + f_2(t)$$

when
$$\frac{\langle f_1 f_2 \rangle}{\langle f_1^2 \rangle} <<1$$

and
$$\frac{\langle f_1 f_2 \rangle}{\langle f_2^2 \rangle} <<1,$$

then
$$< f^2 > \cong < f_1^2 > + < f_2^2 >$$

Here,
$$S/N = 10 \log_{10} S - 10 \log_{10} N$$

and $f(t) = S/N - \langle S/N \rangle$
 $= 10 \log_{10} S - 10 \log_{10} N - \langle 10 \log_{10} S - 10 \log_{10} N \rangle$
 $= 10 (\log_{10} S - \langle \log_{10} S \rangle) - 10 (\log_{10} N - \langle \log_{10} N \rangle)$

Suppose that both the signal and the noise are random, and, furthermore, that the correlation between the two is negligible. In this case, the "signal" is the noise radiated from the target ship as it appears at the position of the listening ship, it therefore includes any distortions introduced by the environment. The "noise" in this case is all other information received by the senar system coming from the same direction as the target. We can then interpret the autocorrelation as the sum of two independent autocorrelations, related to the noise and signal terms. For convenience, these two independent functions have been termed the high- and low-frequency components of the autocorrelation, respectively.

The high-frequency component of the autocorrelation then is a measure of the variation in the noise, while the low-frequency component is a measure of the variation in the signal, induced by its passage through the medium. The lag time at which the autocorrelation crosses the zero axis is the time shift necessary for the signal and the time-shifted signal to become completely uncorrelated.

If the signal is thought of as a pure sinusoid, its autocorrelation would be zero when the two components are out of phase by $\pi/2$. Thus, as an approximation, it may be said that the time at which the autocorrelation crosses zero is equal to one-fourth of the period. If it is assumed that the signal is constant and is modulated by its passage through the medium, then the phenomenon causing the modulation has a period of approximately 600 seconds. If the ship's speed is taken into account, then this phenomenon has a spatial component of approximately

Because the signal we are dealing with is not a pure sinusoid, it is felt that this only gives an indication of the order of magnitude rather than an absolute measure of the size of the phenomenon (internal waves?) causing the modulation. This figure was used as a basis for the internal wave models described in the previous section.



BEARING (AFT IN)

RUN2 LEG2 10,000 YARDS EACH POINT = 2.5 SEC

293°

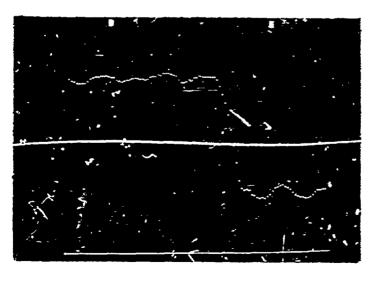
Figure 4-1 Typical DDP-24 Scope Display of Bearing



SPEED (SLOWING FROM 12 TO 5KTS)

RUN2 LEGI 5000 YARDS EACH POINT = 2.5 SEC

Figure 4-2 Typical DDP-24 Scope Display of Speed

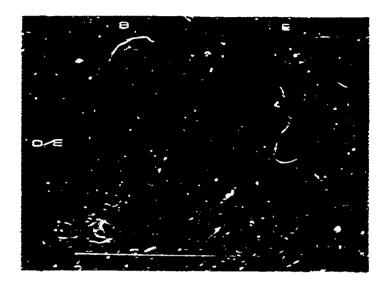


COURSE (SHOWING 20° TURN) 220° RUN2 LEG 2

10,000 YARDS EACH POINT = 7.5 SEC · 阿里里 中心

500°

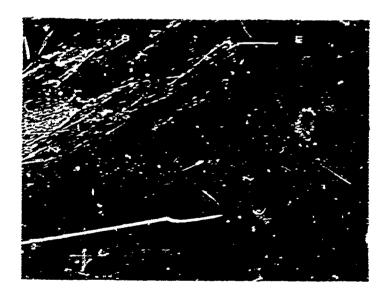
Figure 4-3 Typical DDP-24 Scope Display of Course



D/E ANGLE

RUNI LEG 4 40,000 YARDS (MANUAL—SEARCHING) EACH POINT = 2.5 SEC

Figure 4-4 Typical DDP-24 Scope Display of D/E Angle



S/N

RUN 3 LEG I 5000 YARDS (ATF IN - S/N=+3) EACH POINT = 2.5 SEC

Figure 4-5 Typical DDP-24 Scope Display of S/N

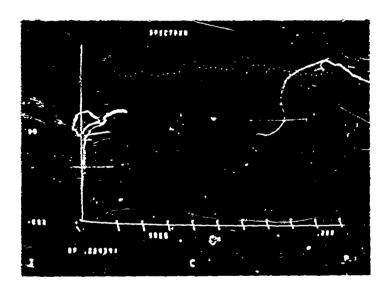


AUTOCORRELATION OF SIGNAL - TO - NOISE

> RUN 3 LEG I 5000 YARDS MAXIMUM LAG=42 SEC

TOTAL SAMPLE IS 420 SECONDS

Figure 4-6 Typical DDP-24
Scope Display of Autocorrelation
of S/N



SPECTRUM OF S/N

RUN 2 LEG I 5000 YARDS

Figure 4-7 Typical DDP-24 Scope Display of Spectrum of S/N

The high- and low-frequency components of the total variance, as determined by autocorrelation analysis, were found to exhibit an interesting effect when examined as a function of range (Figure 4-8). It may be seen from the figure

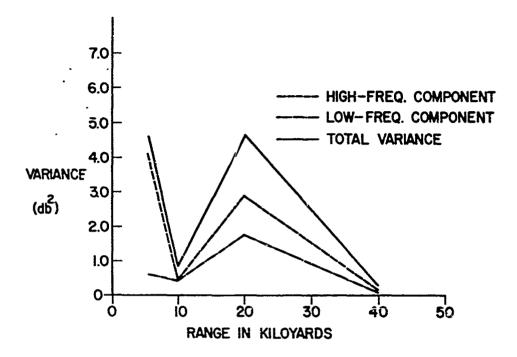


Figure 4-8 Variance of S/N vs. Range

that the two components of variance seem to be related through some sort of feedback loop. When one of these components decreases, the other decreases, and vice versa. This suggests that at least some of the "noise" (high-frequency component) is induced by the system itself and that a high signal variance seems to amplify the system variance. This effect should be studied in more detail, and could lead to an improved sonar capability.

The complete results of the autocorrelation analysis are given in Appendix B.

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CONCLUSIONS AND RECOMMENDATIONS FOR FUTURE WORK

Although a detailed study of the area was made beforehand by examination of records of the Navy and the Hydrographic Office, it required the presence of the oceanographic sensors to delineate the conditions on a rough scale. The combination of the B.T.'s, SVP's, and IRT's determined some of the general characteristics of the area.

This survey, however, was far from sufficient to determine the fine structure of the oceanographic conditions in the area in terms of providing all of the data necessary for an absolute calibration of the tactical propagation models under test. The survey was sufficient to show that the inhomogenieties in the surface channel and the overall structure did exist, and that these were of sufficient magnitude to cause variances in the signal detected by the sonar system employed. These variances, moreover, affected the tactical operation of both the sonar system and the submarine.

The results of the acoustic experiment showed that the SUBIC at-sea ray trace was applicable to active signals as well as to passive signals in predicting average transmission loss terms. In addition, an internal wave ray trace model, programmed on a UNIVAC 1107 computer, explained some of the variance in the S/N as detected by the submarine sonar system. It is important to emphasize that these variances can exist even at ranges as close at 5000 yards and that they are highly dependent on both the overall shape of the SVP and on its spatial and temporal stability.

In order to more effectively utilize the existing sonar system, better and more frequent, and perhaps continuous, sampling of the environment is essential. This will enable accurate predictions of sonar conditions and facilitate passive ranging, either by D/E tracking (from deep convergence zone only), shadow zone (circle chart) tracking⁴, or variance tracking (described below). One suggested method of sampling the environment is described in the following paragraph.

When the submarine arrives in its operating area, it should take a sound velocity profile from the surface to its full depth capability. Based upon this SVP, it chooses the best listening depth and cruises at this depth, taking continuous sound velocity measurements. When the velocity changes by a predetermined amount (ΔV), then a new SVP would be taken. The ΔV would be based upon the environmental history of the area, the time of year, the depth at which the submarine is operating, and possibly other factors. In this way, the submarine may obtain the most up-to-date picture of the environment without interfering with normal ship operations.

For the first time during a SUBIC at-sea test with the DDP-24 computer system, the D/E angle of the sonar system was monitored. Results of this test showed that the vertical beamwidth (13°) of the BQS-6 sonar system was too wide to permit automatic D/E tracking for operation in the surface channel. It is suggested, therefore, that future sonar designs have provision for a narrow vertical beamwidth for tracking, as well as a wide one for search operations.

As a result of the PERMIT experiment, it appears that a passive ranging technique based upon the variance in the signal-to-noise ratio may be feasible. This technique would require an at-sea computer which would be utilized to predict the signal variance at different ranges, as described in Section III. The observed variance of an incoming signal could be measured at several different own-ship depths and compared with the prediction made for these depths. Ideally, there would only be one solution which satisfies all the necessary conditions. Even if this were not so, however, this process would yield additional information which, when combined with circle chart and D/E angle methods, will yield a unique range and depth solution. It is suggested that this procedure be tested on future at-sea experiments.

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APPENDIX A

COMPLETE ATF DATA

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6.750 6812.487 6872.485 68219.	0.000	6.487	6.223 5612.675 6672.673 64926.	0.377	6.157************************************	6.1591 6211.893 6371.892 63224	66.825 6811.937 8871.936 68228.	5.981 6511.861 6871.859 6522E.	5.981	5.959	5.886 6411.623 6471.623 64228	5.784 6011.603 6071.603 60320	5.755 6011.712 60711.005 62205 5.765 6011.712 60711.715 62205	5.828 6411.792 6471.794 6224.	5.89% 6011.885 6071.884 60224	5,981	6.135	6.443	6.685	6.75d 612.642 6472.642 6#219 6.97d 612.858 6672.856 66519	7.234 6818.899 6873.898 69218	7.278 6613.127 6673.125 66218 7.278 6613.629 6673.626 86218	7,322 6613,63; 6673,832 64218 7,388 6613,698 6673,698 66218	7.344 5812.992 6072.998 5219.	7.168 6812.858 68/2.856 68/219	7.836 6812.845 6872.845 88219 6.948 6.948 6812.728 6872.719 68819 6.984 6812.691 6872.691	6,868 612,691 6872,691 68219
136.729 612.487 6872.485 68219.	1.50.000	436.487	145.223 6212.275 6272.273 64925.	4.50.577	120.157"""" SMIL.948 """" BB71.941 AB28E.	436.1991 60111.893 6871.892 6122E	436.525 6811.937 6871.936 68228.	430,047 6011,861 6671,859 66328	435,081	435.959 ED11.772 EB71.771 GB22B.	4.55.886 6811.623 6871.623 68724	455.784 6011.603 6071.603 60320	00111.004 60711.004 60771.003 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200	455.828 6611.755 6671.754 6524.2544.2545.828 6671.754 6524.2544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.2545	435.899 6011.885 6671.884 6622	435,981 6812,816 68228 6822,818 68228	436.135	436.443	436.685	436.75d 612.642 6472.642 6#219 436.97d 612.858 6672.856 665219	437.234 6818,899 6873,898 69218	437.350 613.127 6873.125 68218 437.278 6813.829 6873.826 88318	437,322 6413,43, 643, 6473,83 64218 437,388 6413,498 6421,498	437,344 5812,992 6872,998 6219,	437.168 6812.858 6872.856 68710	437.836 6812.845 6872.845 845 68219 68219 68219 68219 68219 6822.919 68219 68219	436,868 612,691 6472,691 68219
136.729 612.487 6872.485 68219.	1.50.000	436.487	145.223 6212.275 6272.273 64925.	4.50.577	120.157"""" SMIL.948 """" BB71.941 AB28E.	436.1991 60111.893 6871.892 6122E	436.525 6811.937 6871.936 68228.	430,047 6011,861 6671,859 66328	435,081	435.959 ED11.772 EB71.771 GB22B.	4.55.886 6811.623 6871.623 68724	455.784 6011.603 6071.603 60320	00111.004 60711.004 60771.003 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200	455.828 6611.755 6671.754 6524.2544.2545.828 6671.754 6524.2544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.8544.2545.2545	435.899 6011.885 6671.884 6622	435,981 6812,816 68228 6822,818 68228	436.135	436.443	436.685	436.75d 612.642 6472.642 6#219 436.97d 612.858 6672.856 665219	437.234 6818,899 6873,898 69218	437.350 613.127 6873.125 68218 437.278 6813.829 6873.826 88318	437,322 6413,43, 643, 6473,83 64218 437,388 6413,498 6421,498	437,344 5812,992 6872,998 6219,	437.168 6812.858 6872.856 68710	37.036 6012.045 6972.045 6012 36.048 6012.726 672.719 65219 36.064 6612.601 6672.601	436,868 612,691 6472,691 68219
136.729 612.487 6872.485 68219.	1.50.000	436.487	145.223 6212.275 6272.273 64925.	4.50.577	120.157"""" SMIL.948 """" BB71.941 AB28E.	436.1991 60111.893 6871.892 6122E	436.525 6811.937 6871.936 68228.	430,047 6011,861 6671,859 66328	435,081	435.959 ED11.772 EB71.771 GB22B.	4.55.886 6811.623 6871.623 68724	455.784 6011.603 6071.603 60320	00111.004 60711.004 60771.003 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200	1251.1.10 00111.702 00711.704 0524.205.005.005.005.005.005.005.005.005.005	435.899 6011.885 6671.884 6622	435,981 6812,816 68228 6822,818 68228	436.135	436.443	436.685	436.75d 612.642 6472.642 6#219 436.97d 612.858 6672.856 665219	437.234 6818,899 6873,898 69218	437.350 613.127 6873.125 68218 437.278 6813.829 6873.826 88318	437,322 6413,43, 643, 6473,83 64218 437,388 6413,498 6421	437,344 5812,992 6872,998 6219,	437.168 6812.858 6872.856 68710	437.836 6812.845 6872.845 845 68219 68219 68219 68219 68219 6822.919 68219 68219	436,868 612,691 6472,691 68219
6436.729 6412.398 6472.485 64219.	1.50.000	436.487	145.223 6212.275 6272.273 64925.	4.50.577	120.157"""" SMIL.948 """" BB71.941 AB28E.	436.1991 60111.893 6871.892 6122E	436.525 6811.937 6871.936 68228.	430,047 6011,861 6671,859 66328	435,081	435.959 ED11.772 EB71.771 GB22B.	4.55.886 6811.623 6871.623 68724	455.784 6011.603 6071.603 60320	00111.004 60711.004 60771.003 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200	1251.1.10 00111.702 00711.704 0524.205.005.005.005.005.005.005.005.005.005	435.899 6011.885 6671.884 6622	435,981 6812,816 68228 6822,818 68228	436.135	436.443	436.685	436.75d 612.642 6472.642 6#219 436.97d 612.858 6672.856 665219	437.234 6818,899 6873,898 69218	437.350 613.127 6873.125 68218 437.278 6813.829 6873.826 88318	437,322 6413,43, 643, 6473,83 64218 437,388 6413,498 6421	437,344 5812,992 6872,998 6219,	437.168 6812.858 6872.856 68710	437.836 6812.845 6872.845 845 68219 68219 68219 68219 68219 6822.919 68219 68219	436,868 612,691 6472,691 68219
136.729 612.487 6872.485 68219.	1.50.000	436.487	145.223 6212.275 6272.273 64925.	4.50.577	120.157"""" SMIL.948 """" BB71.941 AB28E.	436.1991 60111.893 6871.892 6122E	436.525 6811.937 6871.936 68228.	430,047 6011,861 6671,859 66328	435,081	435.959 ED11.772 EB71.771 GB22B.	4.55.886 6811.623 6871.623 68724	455.784 6011.603 6071.603 60320	00111.004 60711.004 60771.003 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200	1251.1.10 00111.702 00711.704 0524.205.005.005.005.005.005.005.005.005.005	435.899 6011.885 6671.884 6622	435,981 6812,816 68228 6822,818 68228	436.135	436.443	436.685	436.75d 612.642 6472.642 6#219 436.97d 612.858 6672.856 665219	437.234 6818,899 6873,898 69218	437.350 613.127 6873.125 68218 437.278 6813.829 6873.826 88318	437,322 6413,43, 643, 6473,83 64218 437,388 6413,498 6421	437,344 5812,992 6872,998 6219,	017849	437.836 6812.845 6872.845 845 68219 68219 68219 68219 68219 6822.919 68219 68219	436,868 612,691 6472,691 68219
6436.729 6412.398 6472.485 64219.	1.50.000	436.487	145.223 6212.275 6272.273 64925.	4.50.577	120.157"""" SMIL.948 """" BB71.941 AB28E.	436.1991 60111.893 6871.892 6122E	436.525 6811.937 6871.936 68228.	430,047 6011,861 6671,859 66328	435,081	435.959 ED11.772 EB71.771 GB22B.	4.55.886 6811.623 6871.623 68724	455.784 6011.603 6071.603 60320	00111.004 60711.004 60771.003 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200	1251.1.10 00111.702 00711.704 0524.205.005.005.005.005.005.005.005.005.005	435.899 6011.885 6671.884 6622	435,981 6812,816 68228 6822,818 68228	436.135	436.443	436.685	436.75d 612.642 6472.642 6#219 436.97d 612.858 6672.856 665219	437.234 6818,899 6873,898 69218	437.350 613.127 6873.125 68218 437.278 6813.829 6873.826 88318	437,322 6413,43, 643, 6473,83 64218 437,388 6413,498 6421	437,344 5812,992 6872,998 6219,	017849	437.836 6812.845 6872.845 845 68219 68219 68219 68219 68219 6822.919 68219 68219	436,868 612,691 6472,691 68219
6436.729 6412.398 6472.485 64219.	1.50.000	436.487	145.223 6212.275 6272.273 64925.	4.50.577	120.157"""" SMIL.948 """" BB71.941 AB28E.	436.1991 60111.893 6871.892 6122E	436.525 6811.937 6871.936 68228.	430,047 6011,861 6671,859 66328	435,081	435.959 ED11.772 EB71.771 GB22B.	4.55.886 6811.623 6871.623 68724	455.784 6011.603 6071.603 60320	00111.004 60711.004 60771.003 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200 607200	1251.1.10 00111.702 00711.704 0524.205.005.005.005.005.005.005.005.005.005	435.899 6011.885 6671.884 6622	435,981 6812,816 68228 6822,818 68228	436.135	436.443	436.685	436.75d 612.642 6472.642 6#219 436.97d 612.858 6672.856 665219	437.234 6818,899 6873,898 69218	437.350 613.127 6873.125 68218 437.278 6813.829 6873.826 88318	437,322 6413,43, 643, 6473,83 64218 437,388 6413,498 6421,498	437,344 5812,992 6872,998 6219,	017849	437.836 6812.845 6872.845 845 68219 68219 68219 68219 68219 6822.919 68219 68219	436,868 612,691 6472,691 68219

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DEFL ANGL	6.338.6	353.4	358.41	14.0	£358.4	358.4	\$358.4	1358.3	₩353.4	2358.4	Ø358.5	8358.5	4358.5	Ø358.5	Ø358.5	Ø358.5	<b>ß358</b> .5	9353.5	8328	3358.5	1358.5	<b>8358</b> , 5	8358.5	3358.5	8328,5	8358.5	3358.5	358.52	8358.4	<b>3358</b> ; 5	Ø358.5	358,50	353.5	40000	700°00'	1000 C	# 000 F	9358.4	0358.4	Ø358.4	353.5	358,46	1358.4	
N/S	33.67	26.99	67.51	77.	3.63	4.88	34.59	15.25	Ø3.44	2.36	21.31	Ø2.69	45.86	94.18	£3.82	23.27	81.59	\$2.32	15.82	94,12	93.17	33.69	33.57	94.45	ß3.73	g2.23	85.66	45.81	84.112	ij1.93	02.66	U 3. B8	0.00	20°50'5	74.57	22.20	74.7	95.52	02.93	82.25		01.85	Ed1.3647	
3 SPEED	37.47	17.39	Ø7.51	7.58	87.52	97.44	27.43	07.49	7.59	Ø7.58	87.5	87.48	#7.59	97.64	ກັ7. 5ນັ	47.37	87.41	87.59	87.68	47.58	14.79	\$7.39	82.19	07:75	27.68	37.41	մ7.34	7.56	157.71	87.72	7.59	07.39	7.50	7.0	47.02	7 t	04.77	07.62	27.67	87.55	27.44	87.50	8,17,697	; ;
TRUE REARING	195.65	<b>695.53</b>	335.56	. 56	695.55	395.56	ž95.57	895,53	395.59	95.56	155.54	195.58	835.63	35.56	1395.49	195.51	35.54	g95.63	235.58	895.53	195.48	195.51	095.61	095.62	205.58	195.48	895.48	95.53	595.63	895.63	795.59	995.56	297.57	70.00	, 0.0 C C C C C C C C C C C C C C C C C C	10.000	# 0 · 0 # 0 # 0 # 0 # 0 # 0 # 0 # 0 # 0	395.62	395.08	395.54	095.57	\$32°63	8	
ING COURSE	#18#.4	f18g.3	£1815.2	£184.2	11311.2	ğ100.1	0179.9	Ø179.9	179.94	179.33	0179.6	ŭ179.6	2179.7	g179.7	£179.3	g179.g	#179.B	3179.2	179.29	J179.1	0178.8	178.77	0178.9	9179.1	\$179.2	179.92	178.36	9178.7	ນໍ179. ໘	179.28	179.32	9179.2	2.6/10		4140.1	7.77	0.67.78	871,0 7,73.8	8.6/16	9179.7	2179.5	ú179.6	83179.83	
RELATIVE BEARING	#275.1	\$275.2	\$275.3	9275.3	£275.3	0275.4	9275.5	0275.6	9275.6	§275.6	0275.8	\$275.9	4275.9	2275.8	2276.1	\$276.4	3276.5	2276.4	276.29	276.35	3276.6	3276.7	9276,6	1276.4	£276.3	9276.4	276.68	\$276.7	9276.5	\$276.3	9276.2	3276.2	4076.0	4076	2010	7 10 10	26176	32/20	75.7	0275.8	0275.9	g276.g	89275.8D	 
26×	50	17	28	56	95	12	98	τ. 	52-	18	69	78	14 1	19	2.9	55	19	<b>5</b> 3	98	es Cu	97	+1	93	59	26	25	98	94		53	71.	//	† \( \frac{1}{2} \)		2.5	,	^ c	77	52	0.1 :: :: :		14	33	
1X BEARING	ή5.	2.5	815.	15.	21.5	315	٠ د ۲		915.	15.	512	:415	212	915	218	816.	9	816.	<i>3</i> 16.	g16.	g16.	16.	ê 16.	16.	916.	9	210	316		, 10,	3. i	• • • • •	2 5	, v	ָ ער ער	֓֞֝֝֝֓֞֝֝֓֓֓֞֝֝֓֓֓֞֝֝֓֓֓֞֝֓֞֝֓֡֓֓֞֝֓֡֓֞֝֡֓֡֝		, r , r	212	915	015	016	8.6143	
-BEARING 1)	633.95	633. g4	638.13	638.1	658,17	658.21	000000000000000000000000000000000000000	55.05.0	14.859	638.45	638.65	638.72	638.73	653.65	638.09	6 79.25	639.29	638.25	639.09	639.25	639.40	639.53	639.58	5 39 . 29	5 39 . 29	539.25	039.47	6 39 49	0.59	539.24	059.11	11.000	539,00	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	10.000	70.00	000000	100.54	238.61	336,74	538.76	5053.657	
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1	544,41	311.48	3281.4	3179.	52	11,31.1	38.114	23.58	6358.9
	544.41	211.49	\$281.4	8179.	<b>†</b> :	11,11.	17.89	U4.80	5358.9
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	644.33	11.87	2281.3	4179.	()	1,11.,3	37.92	93.44	3359.0
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12.71g         6.592,447         6.57.281         -96.167         -928.21           12.684         6.87.278         6.8179.77         6.92.447         6.57.281         -96.167         -928.21           12.684         6.8272.63         6.8179.77         6.92.461         6.87.287         -95.928         -19           12.684         6.8272.63         6.8186.64         6.92.472         6.92.272         -19         -19           12.599         6.8272.54         6.918.64         6.92.472         6.92.94         -96.193         -19           12.796         6.8272.57         6.918.64         6.92.472         6.92.94         -96.193         -10           12.796         6.8272.57         6.918.64         6.92.472         6.92.442         6.92.94         -96.193           12.596         6.8272.54         6.918.64         6.92.511         -96.193         -92.013           12.797         6.8272.54         6.92.71         -97.11         -97.21         -97.11           12.797         6.8272.54         6.92.71         -97.11         -97.11         -97.11           12.747         6.86.94         6.77.11         -97.11         -97.11         -97.11           12.748         6.92.71		12.85	Ø272.8	J179.6	892.44	07.30	. 25	- 24
12.783		12.71	272.78	1179.7	502.44	7.28	86.16	523.21
12.684         68772.68         68179.77         6892.461         687.287         -85.945         -85.945         -85.945         -85.945         -85.945         -85.945         -85.945         -85.945         -85.945         -85.945         -85.172         -85.162         -19         -85.272         -85.162         -19         -85.272         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.172         -85.	-	12.73	\$272.7	ğ179.7	392.44	07.25	86.22	41,18
12.539         £8872.55         £8188.64         £892.516         £877227         -93.102         -19           12.567         £8272.55         £918.64         £97.172         -6.459         -6.459         -826.193         -19           12.567         £8272.55         £8178.65         £87.172         £87.172         -6.459         -826.193         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10         -10	•	12.63	\$272.6	\$179.7	292.46	87.28	55.94	. 22
12.367		12.53	0272.5	g18g.g	192.51	17.22	13.10	51.
12.576         £3272.39         £3181.87         £392.442         £37.172         -54.252         -525.13         -56.452         -56.412         -56.412         -56.413         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523         -56.523		12.36	\$272.3	g18µ.1	192, 51	17.24	96,19	19
512.574         58772.57         58179.86         5892.442         5877889         -5.439         -6.439         -6.439         -6.439         -6.439         -6.439         -6.439         -6.439         -6.439         -6.439         -6.436         -6.436         -6.436         -6.436         -6.4376         -6.4376         -6.4376         -6.4376         -6.4376         -6.4376         -6.4376         -6.4376         -6.4376         -6.4376         -6.4376         -6.447         -6.636         -6.4376         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616         -6.4616 <td></td> <td>£12.39</td> <td>\$272.3</td> <td>11817.8</td> <td>192.47</td> <td>87.17</td> <td>00° 76</td> <td>333° 96</td>		£12.39	\$272.3	11817.8	192.47	87.17	00° 76	333° 96
\$\text{612.594}         \$\text{6272.59}         \$\text{6179.87}         \$\text{6492.469}         \$\text{647.111}         \$\text{66.523}         \$\text{641.14}           \$\text{612.437}         \$\text{642.521}         \$\text{642.521}         \$\text{642.622}         \$\text{642.623}         \$\text{642.44}         \$\text{642.623}         \$\text{642.623}         \$\text{642.436}         \$\text{642.623}         \$\text{642.123}         \$\text{642.623}         \$\text{642.623}         \$\text{642.623}         \$\text{642.623}         \$\text{642.623}         \$\text{642.623}         \$\text{642.623}         \$\text{642.623}         \$\text{642.123}         \$\text{642.123}         \$\text{642.123}		812.57	\$272.5	0179.8	392.44	87. BB		620.19
\$\beta \times		g12.59	\$272.5	1179.8	192.46	67.11	%6.52	. 22
12.386		12.43	9272.4	118g. g	192.52	57.16	gs. 62	348.14
12.516	=	12.38	\$272.3	3184.1	092.51	67.11	54.82	40,16
12.626		12:.21	272.50	#179.9	1192.43	16.98	06.20	17
\$\begin{array}{c} \text{E} \te		\$12.62	\$272.6	g179.8	,192.44	96.96	56.57	4D. 14
#12.462         ## # ## # ## ## ## ## ## ## ## ## ## ##		\$12.57	9272.5	g179.9	192.49	97.83	63.72	7.17
\$\text{d12.548}\$         \$\text{d12.548}\$         \$\text{d12.548}\$         \$\text{d12.548}\$         \$\text{d12.548}\$         \$\text{d11.749}\$         \$\text{d11.749}\$         \$\text{d11.749}\$         \$\text{d11.749}\$         \$\text{d271.749}\$         \$\text{d271.749}\$         \$\text{d271.639}\$         \$\text{d271.94}\$         \$\text{d271.939}\$         \$\text{d31.749}\$         \$\text{d36.863}\$         \$\text{d46.16}\$         \$\text{d36.863}\$         \$\text{d46.16}\$         \$\text{d36.863}\$         \$\text{d46.16}\$         \$\text{d36.863}\$         \$\text{d46.16}\$         \$\text{d36.863}\$         \$\text{d46.16}\$         \$\text{d66.831}\$         \$\text{d66.831}\$         \$\text{d66.831}\$         \$\text{d66.831}\$         \$\text{d66.832}\$         \$\text{d66.832}\$         \$\text{d66.832}\$         \$\text{d66.832}\$         \$\text{d66.832}\$         \$\text{d66.832}\$         \$\text{d66.832}\$         \$\text{d66.832}\$         <		312.46	\$272.4	n 18g. g	092.49	96.96	07.23	029.17
611.749         6271.74         63179.74         6511.494         66.963         -54.467         -54.64         -65.143         -66.467         -63.467         -63.467         -63.467         -63.467         -63.467         -63.467         -63.467         -63.467         -63.636         -63.637         -63.636         -63.637         -63.636         -63.637         -63.636         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637         -63.637 <t< td=""><td></td><td>312.54</td><td>\$272.5</td><td>g179.3</td><td>192,43</td><td>06.94</td><td>95.32</td><td>928.17</td></t<>		312.54	\$272.5	g179.3	192,43	06.94	95.32	928.17
811.847         84179.84         8411.84         -46.467         -486.467         -486.467         -486.467         -5.657         -486.467         -486.467         -5.657         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.467         -486.468         -486.468         -486.468         -486.468         -486.468         -486.468         -486.468         -486.468         -486.468         -486.468         -486.468         -4		011.74	\$271.7	£179.7	391.49	ige.9	35.14	. 24
11.847		11.84	3271.8	3179.8	វេទ្ធា.ខេន	(6.93	16.46	380
11.859	•	11.84	g271.8	179.97	391.81	36.86	13,000	629, 19
11.99\$	-	11.85	\$271.8	0179:9	361.16	36.83	66.5%	046.16
12:815		11.99	271.98	g179.7	191.16	46.85	37.35	7.
11.994		12:01	9272.0	Ø179.7	591.77	36.89	03.73	19
### 65.771.96 6#271.96 6#271.96 6#271.96 6#272.48 6#272.48 6#272.48 6#45.19 6#5.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48 6#6.48		g11.99	271.98	Ø179.8	691.83	56.81	64:79	626.17
\$12.482		311::36	6271.9	8179.8	591.77	06.70	37.9C	346.16
12:127		12.98	\$272.B	g179.6	91.75	80,	25. 25.	41.004
12, 123 8%272, 12 6179, 645 6.591, 763 6.66, 855 -04, 46822 12:p86		512:13	9272.1	3179.6	391.75	36.8	20,73	92%.19
12:786 68272.03 68179.68 6891.771 686.763 -94.099' 22	ట	77. 12	\$272.1	179.64	791.76	58.96	94.40	77.
	Ø	12:: \$8	ã272.₿	g179.6	291.77	36.76	53	. 22

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846.C4	56.65	10.02 10.02 10.02	26,69	46,59	36,59	36.71	16.60	36.55	96.64	30.7. 60.60	86.68	116.73	46.81	26.79	26.86	26.85	, 00 , 00 , 00 , 00 , 00 , 00	# # # # # # # # # # # # # # # # # # #	10.07	d6.9d	47 67	57.18	17.17	57.11 47.40	14 04	17 77	87.34	87.23	7.25	117.56	7.40	57.4V	27.06	67.38	17.56	17.57	47.43	7.48	17.59	ij7.Ğ1
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11.744	69		1.69	1,,65		300	1.64	1.43	) . 68	72.0	2.74	2.71	2.71	2.72	2.75	 	20.0	7.7	7.0	2000	2 2	2.72	2.78	35	2.11	7 7 7 5	2.73	2.7%	2.71	2.73	200	2.65	200	7	2.71	2.71	2.71	2,74	2,75	2.74
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	643.57		3.18		1288.1	178	.72	31%6.9	87.81	2.7	3358
:	643.55		#8.17		0288.1	117	8.7	11,46.9	47.35	03.3	322
	643.46		38.112		<b>3233.0</b>	117	S	6137.4	18.16	g. 1, g	3,75.5
	77. 1. 25	ŧ	J7.66		1287.6	ú 17	4.6	11,77,1	ú8.19	65.3	558
	642.83		\$7.45		5287.4	£#17	9.7	3187.1	88.113	37.2	558
	642.92	1	87.58		\$287.5	117	4.6	31.57.8	07.77	52.8	338
	643.11		87.79		5287.7	317	9.5	3187.15	37.77	3.7	3328
•	642.96		47.61		3287.6	317	9.5	31:37.1	J8. N9	000	3358
	642.45		J7.23		4287.2	218	13 23	5187.2	53.24	33.6	1558
	542.28		7.0		U287. B	318		1137.2	8.112		3,35
	642.59		17.31		\$287.3	317	9.7	137.69	47.77	81.2	1358
	642.89		\$7.53		2287.5	Ø17	9.5	3137.1	87.83	83.4	358
	642.67		27.43		3237.4	179	. 32	81:77.2	88.13	83.8	1358
	642.26	,	27.56		3237.6	513	5.1	5137.2	38.23	5,4	558
	542.19		17. 32		3287.5	213	ğ.1	3137.1	36.73	85.1	358
	642.61		97.36		\$287.3	517	9.7	3127.6	87.77	7.	3.358
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	542.65		27.43		287.49	179	. 32	11:17.2	28.15	٠ د	3320
	642.33		\$7.14		287.13	318	д. 23	1157.2	<b>183.16</b>		53.5
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	642.25		67.59		1287.5	Ø17	5.5	7137.0	57.85	7	2528
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	642.39		37.54		8287.5	317	9.5	8187.1	38.88	31.4	0358
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	642.96		Ø7.68		5287.6	179	. 33	าฮุ?.ฮา	87.86	J	3.53
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,	643.16		57.87		\$287.8	617	9.1	8187.B	118.63	***	3.28
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	4.04	70.75	7.7	117.98	08,11	17.93	87.73	17.78	118,11	53.14	<b>87.92</b>	17.74	87.81	117.98	18.112	11.92	37.75	87.78	47,94	d8. g3	¥7.94	67.72	:17.68	47.89	188. <b>g</b> 3	£7.94	37.77	¥7.74	17.84	47.93	67:93	£7.88	147.181	12.84	17.89	662.703	17.83	67.83
	7.00.1	200	9186.2	3116.2	3136.1	11186.1	ชาธ์6.1	4116.2	ยังฮัย	0126.1	3156.	196.13	1186.1	3106.1	1126.2	8126.3	g186.n	#1#6.1	8186.B	4186: b	8185.9	31 y 5. y	31 BG. 13	Ø156.1	1186. S	\$185.9	3136.18	1126.1	#186.1	91%6.1	31 36.1	d156.1	£96.17	1186.1	1186.1	8156.177	£36.12	#156.1
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	900	316.47	Ø16.47	616.22	816.19	16.11	8:16.2g	Ø15.95	g15.62	<b>£15.56</b>	Ø15.63	Ø15.78	315.77	815.55	\$15.42	\$15.39	115.53	115.55	815.33	815.85	¥14.99	Ø15.26	Ø15.45	#15.35	Ø15.01	Ø15. \$3	¥15.48	Ø15.75	Ø15.79	\$15.76	315.84	Ø15.95	815.97	816.98	Ø16.Ø6	1,6	316, 16	#16.3#
-	1470	641.14	641.53	541.33	141.25	64.1.27	64125	641.15	644.83	645.74	641.72	64ď.76	644.78	6416.74	643,59	64 %. 63	6411.73	6411.65	643.43	645,23	6416.23	6436.39	641,54	6411.54	640.23	645.21	64 y . 59	641.81	64ÿ.37	6443.83	641.94	644.93	644.96	641. N3	64.1.37	1.49	641.16	641.33

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Total Control

-0356.65	356.63	2375	356.74	1356.5	4356.6	3556.7	2356.6	356.7	(350°C)	2356.6	1356.7	2556.6	2556.7	7,000,00	1,356,3	356.31	3556.8	1356.3	2356.7	2556.7	0356.7	0.350.0	3.10.01	/\.\.\.\.\.\.\.\.\.\.\.\.\.\.\.\.\.\.\.	4256.6	2356.6	1356.7	0.356.6	0.3563	U356.6	2 2 2 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	6356.7	2556.6	356-66	3356.6	5356.7	0.356.6	8 350 °C	2.556.7	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	0 4 5 C C C C C C C C C C C C C C C C C C	) ( ) ( ) 1 ) 1	
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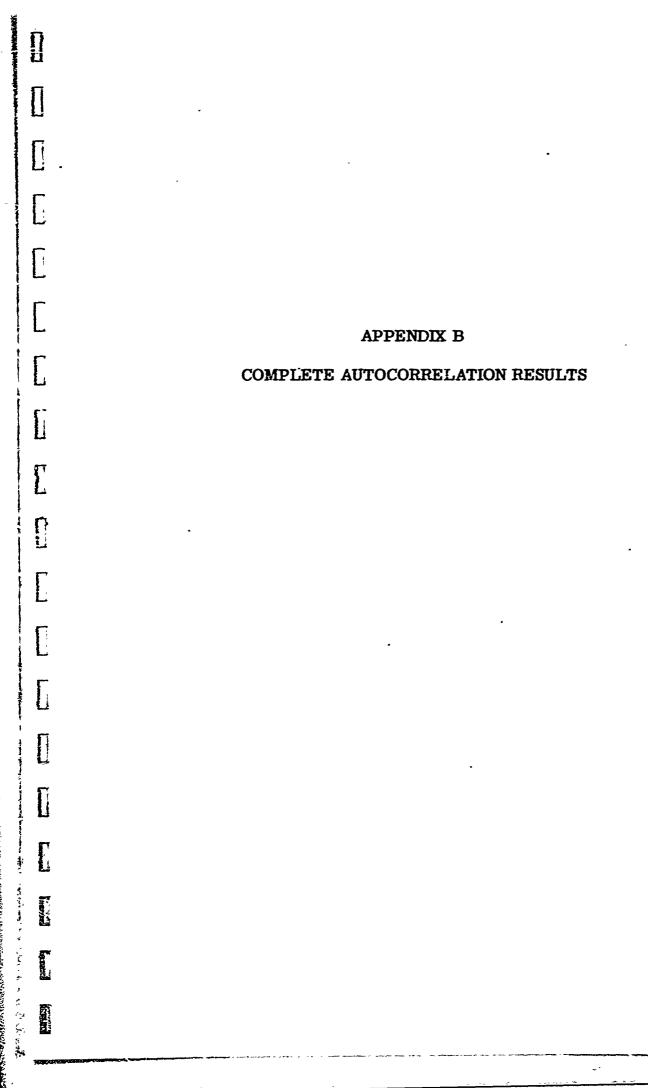
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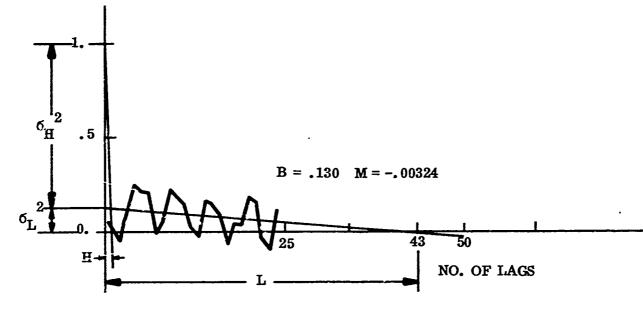
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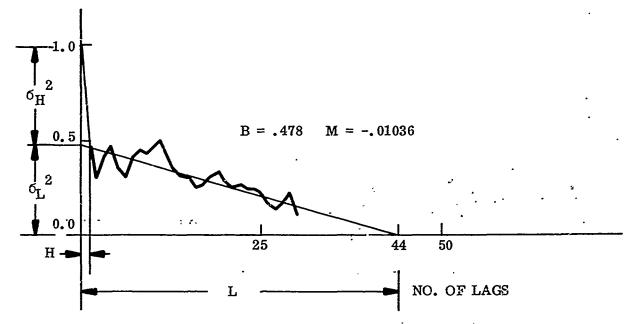
SIMPLIFIED AUTOCORRELATION FUNCTIONS NORMALIZED VARIANCE VS. TIME (EACH LAG = 2.5 SEC)



RUN 2 LEG 1 SIGNAL-TO-NOISE 5,000 YARDS DATA BASED ON 247 SELECTED FRAMES (617 SECONDS), 10% LAG

= 2.5 SEC

SIMPLIFIED AUTOCORRELATION RESULTS NORMALIZED VARIANCE VS. TIME



$$6_{L}^{2} = 48\% = 0.413$$
 $6_{L} = 0.642$
 $6_{H}^{2} = 52\% = 0.449$
 $6_{H}^{2} = 0.668$
 $6_{T}^{2} = 0.86 = VARIANCE$
 $6_{T}^{2} = 0.926$
 $6_{T}^{2} = 0.926$

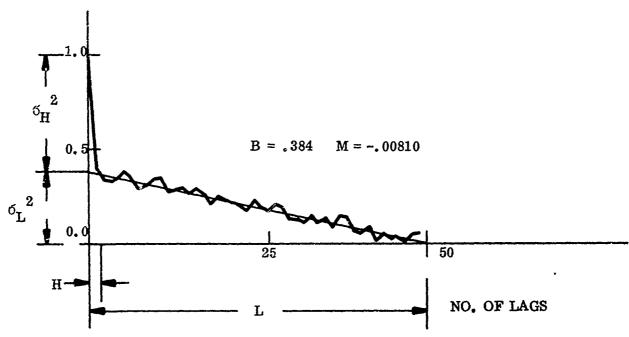
RUN 2 LEG 2 SIGNAL-TO-NOISE

10,000 YARDS

DATA BASED ON 308 FRAMES

(ENTIRE RUN) OR 770 SECONDS WITH 10% LAG

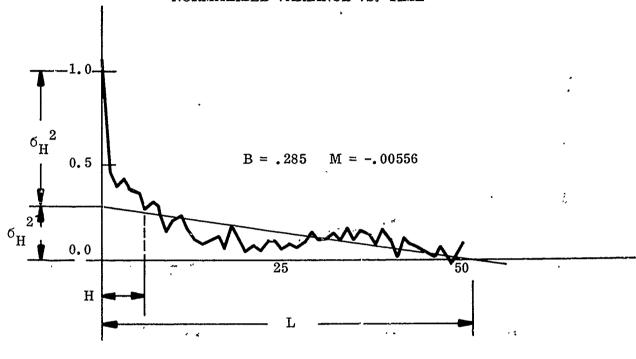
SIMPLIFIED AUTOCORRELATION RESULTS NORMALIZED VARIANCE VS. TIME



$$6_{L}^{2} = 38\% = 1.77$$
 $6_{L} = 1.33$
 $6_{H}^{2} = 62\% = 2.89$
 $6_{H}^{2} = 4.66 = VARIANCE$
 $6_{L}^{2} = 2.16$
 $6_{L}^{2} = 1.70$
 $6_{L}^{2} = 1.70$

RUN 2 LEG 3 SIGNAL-TO-NOISE 20, 000 YARDS DATA BASED ON 467 FRAMES (ENTIRE RUN) OR 1170 SECONDS WITH 10% LAG

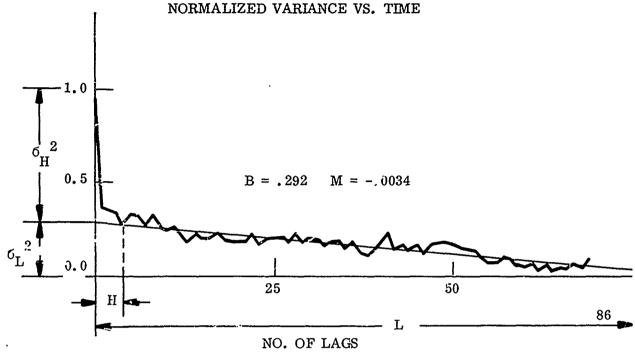
SIMPLIFIED AUTOCORRELATION FUNCTIONS NORMALIZED VARIANCE VS: TIME



$$6_{L}^{2} = 28.5\% = .077$$
 $6_{L}^{2} = 71.5\% = .193$
 $6_{H}^{2} = 0.27 = VARIANCE$
 $6_{H}^{2} = .439$
 $6_{T}^{2} = 0.27 = VARIANCE$
 $6_{T}^{2} = .509$
 $6_{T}^{2} = .509$

RUN 2 LEG 4 SIGNAL-TO-NOISE 40,000 YARDS DATA BASED ON 505 FRAMES (ENTIRE RUN) - 1266 SECONDS, 10% LAG

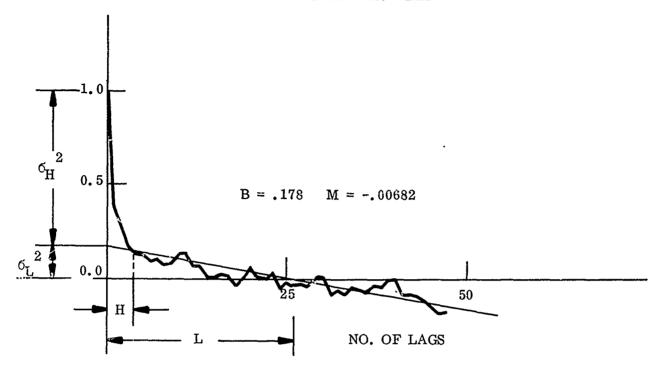
SIMPLIFIED AUTOCORRELATION FUNCTIONS NORMALIZED VARIANCE VS. TIME



$$6_{L}^{2} = 29\% = .246$$
 $6_{L}^{2} = 71\% = .604$
 $6_{H}^{2} = 0.85 = VARIANCE$
 $6_{T}^{2} = 0.85 = 0.85$
 $6_{T}^{2} = 0.85$

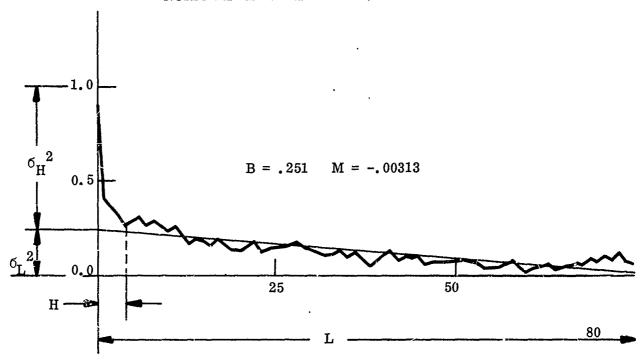
RUN 2 CLOSING SIGNAL-TO-NCISE DATA BASED ON FIRST 693 FRAMES (1730 SECONDS), 10% LAG

SIMPLIFIED AUTOCORRELATION FUNCTIONS NORMALIZED VARIANCE VS. TIME



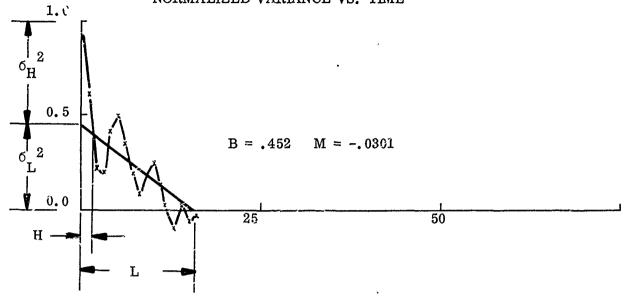
RUN 2 CLOSING SIGNAL-TO-NOISE DATA BASED ON 476 FRAMES (693-1169) - 1190 SECONDS, 10% LAG

SIMPLIFIED AUTOCORRELATION FUNCTIONS NORMALIZED VARIANCE VS. TIME

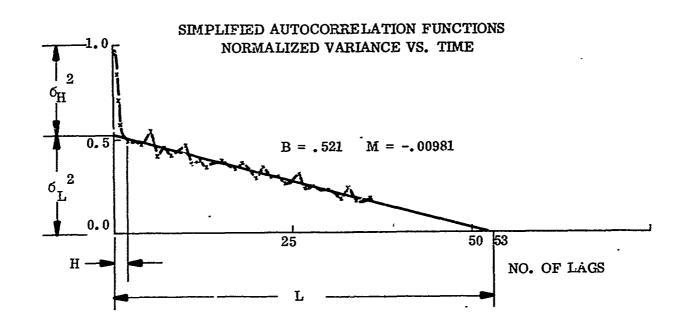


RUN 2 CLOSING SIGNAL-TO-NOISE DATA BASED ON 792 FRAMES (0-792) 1980 SECONDS, 10% LAG

SIMPLIFIED AUTOCORRELATION RESULTS NORMALIZED VARIANCE VS. TIME



RUN 3 LEG 1 SIGNAL-TO-NOISE DATA BASED ON 175 FRAMES (ENTIRE RUN) OR 435 SECONDS (10% LAG)

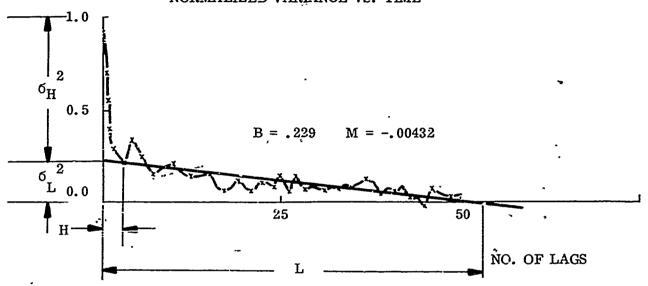


$$6_{L}^{2} = 52\% = 4.16$$
 $6_{L} = 2.04$
 $6_{H}^{2} = 48\% = 3.85$
 $6_{H} = 1.96$
 $6_{T}^{2} = 8.01 = VARIANCE$
 $6_{T}^{2} = 8.01 = VARIANCE$
 $6_{T}^{2} = 2.83$
 $6_{T}^{2} = 2.83$

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RIN 3 LEG 2 SIGNAL-TO-NOISE 10,600 YARDS DATA BASED ON 364 FRAMES (ENTIRE RUN) - (910 SECONDS) 10% LAG

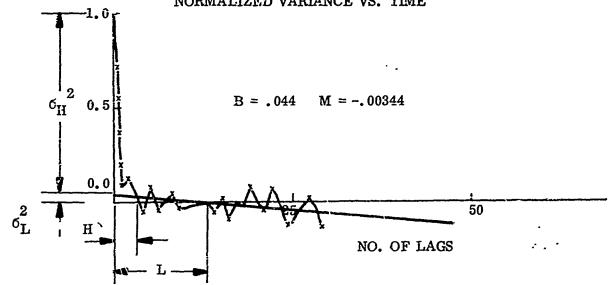
SIMPLIFIED AUTOCORRELATION FUNCTIONS -NORMALIZED VARIANCE VS. TIME



$$6_{L}^{2} = 23\% = 1.24$$
 $6_{L}^{2} = 77\% = 4.15$
 $6_{H}^{2} = 5.39 = VARIANCE$
 $6_{T}^{2} = 5.39 = VARIANCE$
 $6_{T}^{2} = 2.32$
 $6_{T}^{2} = 2.32$

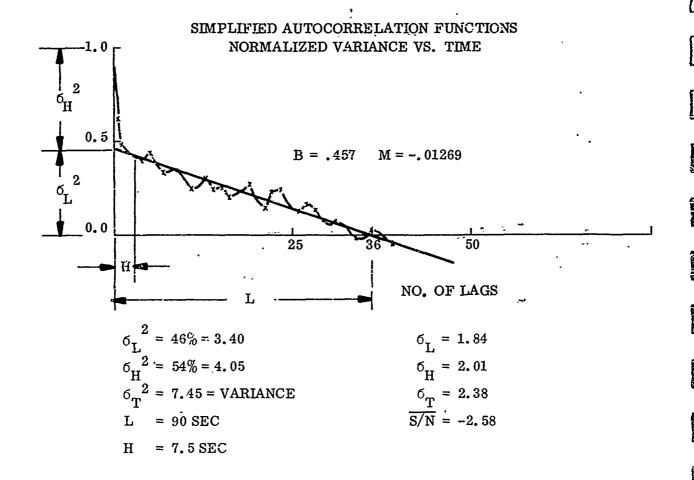
RUN 3 LEG 3 SIGNAL-TO-NOISE 20,000 YARDS DATA BASED ON 508 FRAMES (ENTIRE RUN) - 1270 SECONDS, 10% LAG

SIMPLIFIED AUTOCORRELATION FUNCTIONS NORMALIZED VARIANCE VS. TIME

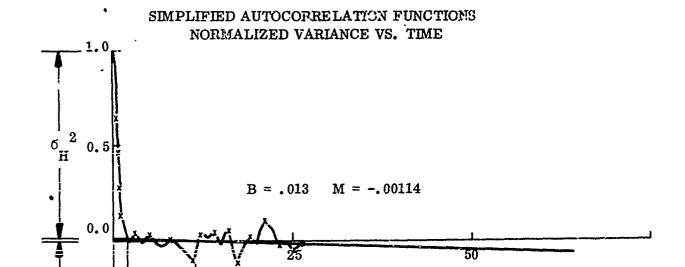


RUN 3 LEG 4 SIGNAL-TO-NOISE 40,000 YARDS DATA BASED ON 296 FRAMES (043 TO 339) - 740 SECONDS, 10% LAG

= 7.5 SEC

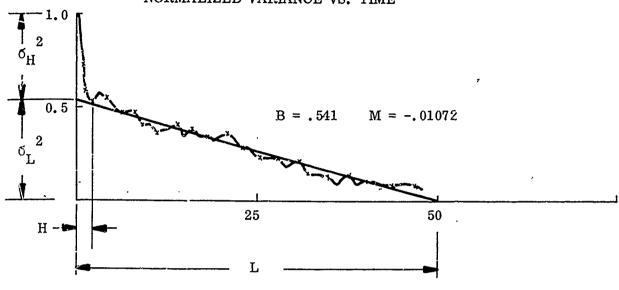


RUN 3 LEG 4 SIGNAL-TO-NOISE 40,000 YARDS DATA BASED ON 393 FRAMES (ENTIRE RUN) - 980 SECONDS, 10% LAG



RUN 3 LEG 5 SIGNAL-TO-NOISE 60,000 YARDS DATA BASED ON 266 FRAMES (035-300) 665 SECONDS, 10% LAG

SIMPLIFIED AUTOCORRELATION FUNCTIONS NORMALIZED VARIANCE VS. TIME



$$5_{T}^{2} = 54\% = 5.55$$

$$6_{L} = 2.35$$

$$6_{xx}^{-2} = 46\% = 4.71$$

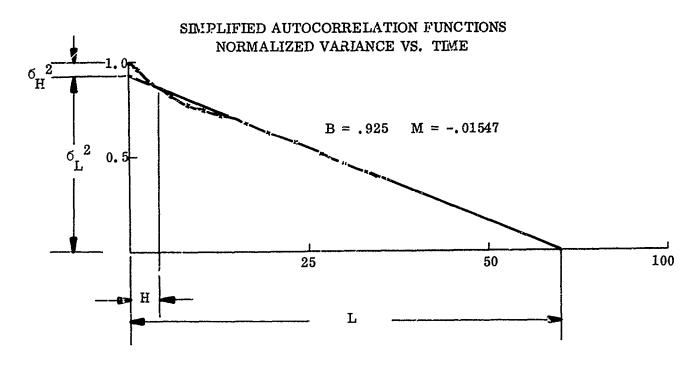
$$6_{H} = 2.17$$

$$6_{\text{T}}^2 = 10.26 = \text{VARIANCE}$$

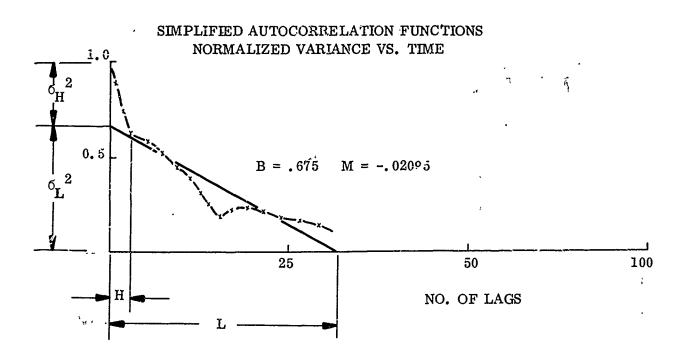
$$6_{\rm T} = 3.20$$

$$L = 125 S \tilde{E} C$$

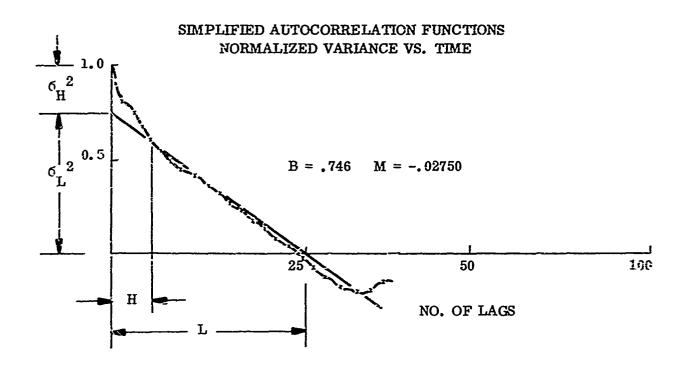
RUN 3 LEG 5 SIGNAL-TO-NOISE 60,000 YARDS DATA BASED ON 484 FRAMES (ENTIRE RUN) - 1210 SECONDS, 10% LAG



RUN 2 LEG 4 (BEARING) 40,000 YARDS DATA BASED ON 346 FRAMES (114-460) - 865 SECONDS, 10% LAG



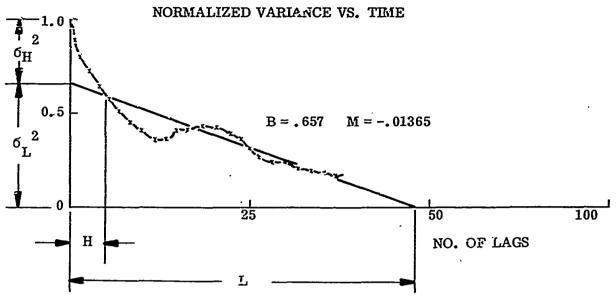
RUN 3 LEG 4 (D/E) 40,000 YARDS DATA BASED ON 317 FRAMES (076-393) 792 SECONDS, 10% LAG



$$6_{L}^{2} = 75\% = .00281$$
 $6_{L} = .0530$
 $6_{H}^{2} = 25\% = .000938$
 $6_{T}^{2} = .00375 = VARIANCE$
 $6_{T}^{2} = .0612$
 $6_{T}^{2} = .0612$
 $6_{T}^{2} = .0612$
 $6_{T}^{2} = .0612$

RUN 3 LEG 4 (BEARING)
40,000 YARDS
DATA BASED ON 393 FRAMES
(ENTIRE RUN) - 980 SECONDS, 10% LAG

SIMPLIFIED AUTOCORRELATION FUNCTIONS

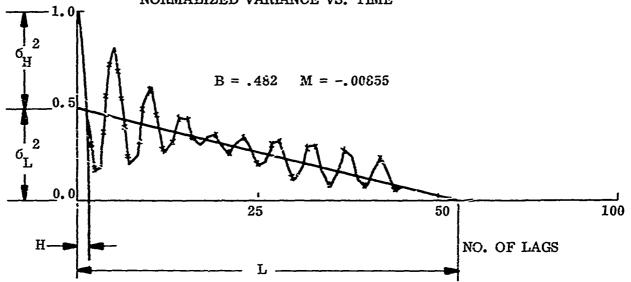


$$6_{L}^{2} = 66\% = .00629$$
 $6_{L}^{2} = 34\% = .00323$
 $6_{H}^{2} = .00952 = VARIANCE$
 $6_{T}^{2} = .00952 = VARIANCE$
 $6_{T}^{2} = .00952 = VARIANCE$
 $6_{T}^{2} = .00952 = VARIANCE$

= 12.5 SEC

RUN 3 LEG 5 (D/E) 60,000 YARDS DATA BASED ON 386 FRAMES (0-386) - 965 SECONDS, 10% LAG

SIMPLIFIED AUTOCORRELATION FUNCTIONS NORMALIZED VARIANCE VS. TIME



$$6_{\tau}^{2} = 48\% = .00786$$

$$\sigma_{L} = .0886$$

$$6^2 = 52\% = .00852$$

$$6_{\rm H} = .0923$$

$$\frac{6}{T}^2 = .0164 = VARIANCE$$

$$\sigma_{\rm T} = .128$$

$$L = 132 SEC$$

$$H = 3.75 SEC$$

RUN 3 LEG 5 (SPEED)
60,000 YARDS
DATA BASED ON 454 FRAMES
(ENTIRE RUN) - 1135 SECONDS, 10% LAG

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